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OPTICAL TECHNOLOGY DIVISION

PROJECT MEMORANDUM

PM-1550-X

7 APRIL 1975

SENSOR SYSTEM POST FLIGHT REPORT

SV-9 (S/N 012)

Prepared by:

Flight Operations and Evaluation Section

Reviewed by:

F.L. HARRIGAN,/JR., Manager

Flight Operations and Evaluation

Approved by:

W.C. COTTRELL, Manager

Field Operations Department

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PROJECT MEMORNADUM NUMBER:

PM-1550-X

PREPARED BY:

Flight Operations & Evaluation

DATE:

7 April 1975

SUBJECT:

Sensor System Post Flight Report

SV-9 (S/N 012)

DISTRIBUTION:

SP-7 (2) WCF0 (2)

Maj.Berganini)

SSC/DCO R. Jones

W. Keeney

J. Garrish P. Petty

C. Karatzas

U. Najaika

L. Weeks

ABSTRACT:

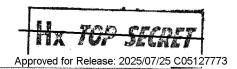
This report outlines the flight history

for the SV-9 (S/N 012) Sensor System.

DESCRIPTORS:

Flight Report, S/N 012

Flight Operations, S/N 012



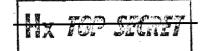
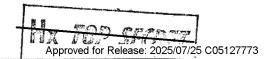
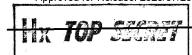


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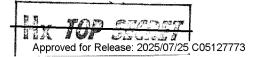
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MISSION 1209

SENSOR SYSTEM OPERATION

POST FLIGHT REPORT

1.0 INTRODUCTION

I.I Mission Objective

The primary objective of the Hexagon Mission is to provide high resolution photography. The intent of the ninth flight was to demonstrate functional operation of the primary satellite vehicle 120 day capability. This objective was surpassed with an active mission life of 130 days.

1.2 Mission Description

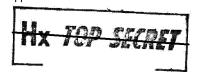
The Hexagon Mission 1209 satellite vehicle was launched from VAFB, SLC-4E, at 1130 PST 29 October 1974 using a Titan 3D booster vehicle. All recovery vehicles were successfully air retrieved within predicted impact dispersions. Recoveries were Day 19, 55, 84 and 130 respectively.

Operational photography began on Rev 6, Mission Op 4 and continued with no camera system malfunctions throughout the mission. The Aft camera film supply was depleted on Rev 2086, Mission Op 757. The Foward camera film supply was depleted on Rev 2090, Mission Op 759.

Evaluation of RV-I photography indicated a need to change the Aft camera OOAA in-track nominal from -3 steps to -7 steps. This change was made on Mission Op 156. Evaluation of Rv-2 photography indicated a need to change the Forward camera OOAA in-track nominal from -3 steps to -2 steps. This change was made on Mission Op 390.

The Aft camera film supply contained three segments of SO-255 color film and one segment of SO-130 IR color film. The lengths and operational intervals associated with these segments were as follows:

SO-255	2775 ft	Ops 162-183	Revs 378-431
S0-255	2875 ft	Ops 314-345	Revs 754-818
SO-255	2500 ft	Ops 458-471	Revs 129-1177
SO-130	3400 ft	Ops 514-530	Revs 1275-1320



1.2 Mission Description - Cont'd.

The active photographic mission was terminated with Rv-4 recovery on day 130 following depletion of both film supplies. A solo phase of the mission extended the vehicle life to day 141, at which time the vehicle was deboosted and re-entered.

1.3 Mission Highlights

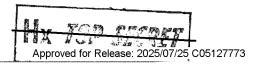
Sensor System highlights of the mission can be summarized as follows:

- a. The Sensor System demonstrated a functional orbital life of 130 days.
- b. Both Forward and Aft cameras utilized 100% of their respective film supplies. Approximately 98% of the available pneumatics was expended.
- c. The Sensor System demonstrated the capability to operate satisfactorily with SO-130 Infrared color film and SO-255 color film in the Aft camera.
- d. A stellar photography experiment was demonstrated on Rev 1769, Mission Op 713.
- e. The image quality for both cameras ranged from very good to poor during the mission; the poor being attributable to atmospheric conditions, photography at both high and low solar elevations and climatic conditions associated with winter missions. The image quality of 1209 compared with previous missions, and there was a preference for the Aft camera imagery when compared to the Forward.

Figure I-I presents a graphic history of remaining system life percentages throughout the mission.

1.4 Launch Configuration

- a. Mission Operation Number 1209
- b. Intra-range Operation No. 7122
- c. Satellite Vehicle SV-9
- d. Sensor System S/N 012
- e. Sensor System Configuration





1.4 Launch Configuration - Cont'd.

	Forward Camera	Aft Camera
Filter Types	W-12	W-12
Focal Length	60.0041 in.	59.9906 In.
Focus Setting	31 Microns	70 Microns
OOAA Setting		
In-Track	-3 CMD Steps	-3 CMD Steps
Cross-Track	+3 CMD Steps	-3 CMD Steps
Film Type	1414	1414/\$0-255/\$0-130
Film Length	116,930	111,958
Film Weight	920.0 lbs.	914.4 lbs.
Spool Number	5052	5048
Pneumatics Loaded	34.81	bs.

1.5 Launch and Orbital Parameters

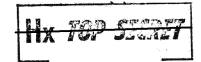
	Planned	Actual
Launch Time-GMT	1930Z	1930Z
Launch Time-SVT	67.0	67.0
Inclination-degrees	96.8	96.7
Initial Perigee-n.miles	87.1	85.3
Initial Apogee-n.miles	151.8	155.6
Argument of Perigee-		
degrees	160,2	163.3
Initial Period-minutes	88.89	88.94

Table I-I and Figure 1-2 define the basic orbital parameter considerations for the active mission. Fifty-one orbit adjusts were performed.

1.6 Mission Film Usage Summary

The distribution of film footage as functions of the various operating modes is presented in Figures 1-4 to 1-21. The mission segment to segment film usage is summarized as follows:

	Rev Span	Camera	Recovered			
RV-I	Launch+307	Forward Aft	29512 29576			
RV-2	308-888	Forward Aft	29537 26886			
RV-3	889-1358	Forward Aft	28505 27652			
RV-4	1359-2090	Forward Aft	29250 27733			
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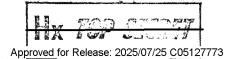


1.6 Mission Film Usage Summary-Cont'd.

Of this footage, the engineering and other non-intelligence operations consumed approximately 4400 and 4408 feet for the A and B sides, respectively, as summarized in the following:

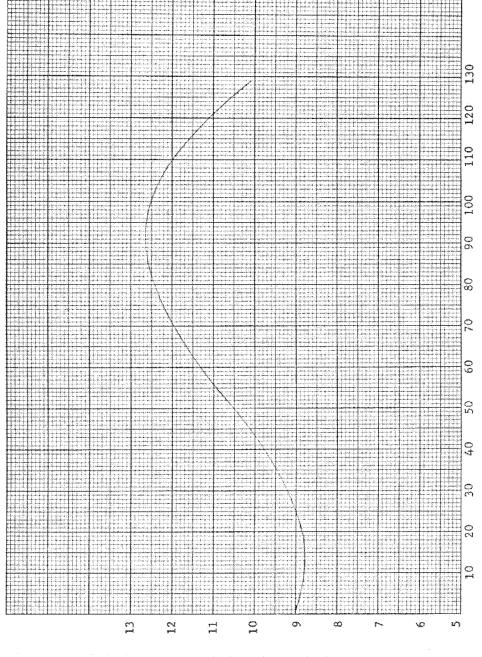
1209 Non-Intelligence

•	Forward Camera	Aft Camera
Pre-Launch	1601	1609
RV-I Engineering	983	983
RV-2 Engineering	726	726
RV-3 Engineering	541	541
RV-4 Engineering	549	54 9
Total Utilization	4400	4408
Film Recovered	116804	111847
PCT. Non-Intelligence	3.77	3.94



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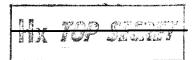
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ISSION DAY

BELY ANGLE (DEGS)

FIG. 1-2 BETA ANGLE VS MISSION DAY



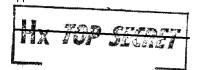
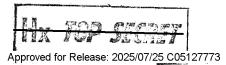


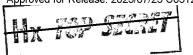
TABLE 1 - 1

BASIC ORBITAL PARAMETERS

DAY	REV	PERIOD	PERIGEE	APOGEE	INC. AF	G/PER	B ANG
L/0 0	NOM I	88:54 88:57	87.3 85.3	152.5 155.8	96.8 96.7		9.0 9.0
1	8	88:56	85.4	154.8		66.0	9.0
2	24	88.52	85.0	152.4		61.6	9.0
3	40	88:48	84.8	150.0		57.1	8.9
4	57	88:44	84.7	147.3	96.7	52.2	8.9
OA# I	63	20 10	87				
5 6	73	88:49	87.9	5 .5 49.5		41.3	8.9
7	89 105	88:45 88:40	87.8 87.7	149.3		37.2 33.0	8.9 8.9
OA# 2	112	00:40	01 4.1	147.5	30.7 1	٠,٠٠٠	0.9
8	122	88:51	88.0	155.7	96.7 I	36.8	8.8
9	142	88:47	87.8	153.1	96.7 i	31.9	8.8
10	154	88:44	87.8	151.3		28.7	8.8
OA# 3	159					****	
1	170	88:52	88.0	157.6	96.7 1	30.9	8.8
12	186	88:47	87.9	154.9			
13	203	88:42	87.7	152.4		22.5	
14	219	88:37	87.4	149.5	96.7	18.6	8.8
OA# 4	224						
15	235	88:55	87.8		96.7		
16 OA# 5	251 257	88:50	87.7	160.3	96.7 1	21.0	8.8
	259						
17	268	88:49	87.9	152.7	96.7 1	37.6	8.8
18	284	88:45	87.9	151.0		33.4	8.8
OA# 7	286	0.04 4.2	47.47	1.21.10	20.7	m/ w1 % 13	0,0
19	300	89:04	88.0	166.0	96.7	38.8	8.9
20	316	89:00	88.0	163.9		34.8	9.0
0A# 8	322						
21	332	88:49	88.0	155.1	96.7	31.2	8.9
22	349	88:44	88.0	152.7		26.8	8.9
23	365	88:40	87.7	150.2	96.7 1	22.8	9.0
OA# 9	37.0						
24	381	88:51	87.8	159.5		26.5	9.0
25	397	88:47	87.7	157.0		22.6	9.0
26 0A#10	413 420	88:43	87.5	154.5	96.7	18.7	9.1
27	430	88:52	87.7	161.4	96.7 1	20.4	9.1
28	446		87.5	158.9		16.6	9.1
29	462	88:42	87.1	156.1		12.9	9.2
			5 ,		2 1		30° 40° 4000



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TABLE I - I Cont'd.

BASIC ORBITAL PARAMETERS

heems.	DAY	REV	PERIOD	PERIGEE	APOGEE	INC.	ARG/PER	B ANG
	OA#11	467						
motivi	0A#12	469						
	30	478	88:52	88.0	155.9	96.7	137.8	9.2
	31	494	88:48	88.0	153.9	96.7	133.6	9.3
	32	511	88:44	88.0	151.8	96.7	129.2	9.3
o'Phone	OA#13	517	JJ.,		12110		, ,	* * *
	33	527	88.50	87.7	157.3	96.7	129.6	9.4
	34	543	88:46	87.8	155.1	96.7	125.1	9.4
opening.	35	559	88:42	87.6	152.4	96.7	121.2	9.5
	0A#14	565	001,2	0,,,0	, , ,			
	36	576	88:52	87.8	160.4	96.7	123.6	9.6
itmin	37	592	88:47	87.7	158.2	96.7	119.7	9.6
	38	608	88:43	87.5	155.9	96.7	115.9	9.7
	OA#15	614	00.75	0,13	12212	50.	, , , , ,	* * '
	0A#16	616						
infrance .	39	624	88:51	88.1	155.2	96.7	137.9	9.7
	40	640	88:48	88.1	153.3	96.7	133.8	9.8
	41	6.57	88:44	88.1	151.0	96.7	129.3	9.9
petiting	OA#17	662	00.444	30.1	12110	30.,	, , , , ,	2.4.2
	42	673	88:49	87.9	156.3	96.7	129.2	9.9
	43	689	88:45	87.7	153.9	96.7	125.3	10.0
-	44	705	88:41	87.6	151.4	96.7	121.4	10.1
	OA#18	711			****			
	45	722	88:53	87.9	161.0	96.7	124.7	10.2
	46	738	88:49	87.7	158.9	96.7	120.9	10.2
- Andrews	47	754	88:45	87.6	156.7	96.7	117.1	10.3
	OA#19	759	00713	V , L L	a are man ar r	, , ,	. , . , .	
	48	770	88:50	87.8	161.0	96.7	117.3	10.4
Martin.	49	786	88:46	87.6	158.8	96.7	113.6	10.5
	50	803	88:41	87.3	155.8	96.6	109.6	10.5
	0A#20	808						
ma	0A#21	810						
	51	819	88:51	87.9	154.6	96.6	137.6	10.6
	52	835	88:46	87.7	152.2	96.6	133.5	10.7
	53	851	88:41	87.6	149.7	96.6	129.5	10.8
	OA#22	857						
	54	868	88:51	88.0	157.1	96.6	133.0	10.8
	55	884	88:47	88.0	154.9	96.6	128.8	10.9
of-con	56	900	88:43	87.7	152.3	96.6	124.8	11.0
	0A#23	906	,-			, -		
	57	916	88:52	87.9	159.3	96.6	126.8	11.1
	58	932	88:47	87.8	156.8	96.6	122.9	11.1
	59	949	88:42	87.5	153.8	96.6	118.6	11.2



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TABLE 1 - 1 Cont'd.

BASIC ORBITAL PARAMETERS

DAY	REV	PERIOD	PERIGEE	APOGEE	INC.	ARG/PER	B ANG
OA#24	961						
6.0	965	88:54	87.9	162.5	96.6	123.1	11.3
61	981	88:49	87.9	160.0	96.6		11.4
62	997	88:45	87.7	157.4	96.6		11.4
DA#25	1003	00113	V , , ,		,,,,		
OA#26	1005						
63	1014	88:50	88.1	154.2	96.6	137.4	11.5
64	1030	88:46	87.9	152.1	96.6	133.2	11.6
65	1046	88:42	87.9	149.8	96.6	129.1	11.6
)A#27	1052	09.142	07.9	147.0	90.0	122.1	11.0
56 56	1052	88:53	88.0	158.3	96.6	132.0	11.7
				156.2	96.6	128.1	11.8
67	1078	88:49	88.0			123.7	11.8
68	1095	88:44	87.8	153.2	96.6	123.1	11.0
DA#28	1100	00.70	07.0	150 0	0.6	125 0	110
69	1111	88:50	87.9	158.9	96.6	125.0	11.9
7.0	1127	88:45	87.7	156.0	96.6	121.2	12.0
71	1143	88:40	87.4	152.9	96.6	117.3	12.0
A#29	1149	0.0	A	163.0	20.4	101 5	10.1
72	1159	88:52	87.9	161.8	96.6	121.5	12.1
73	1176	88:48	87.7	159.1	96.6		12.1
74	1192	88:43	87.4	156.5	96.6	113.5	12.2
)A#30	1198			*			
DA#31	1200						
75	1208	88:52	87.9	155.7	96.6	138.0	12.2
76	1224	88:48	87.9	153.6	96.6	133.9	12.3
77	1241	88:42	87.7	150.4	96.6	129.4	12.3
)A#32	1246						1 46 2
78	1257	88:49	87.9	155.6	96.6	131.6	12.4
79	1273	88:44	87.7	152.9	96,6	127.6	12.4
80	1289	88:39	87.5	149.9	96.6	123.7	12.4
)A#33	1295						
81	1305	88:53	87.9	159.4	96.6	128.6	12.5
82	1322	88:48	87.8	156.6	96.6	124.3	12.5
8.3	1338	88:43	87.6	153.9	96.6	120.3	12.5
)A#34	1344						
84	1354	88:53	87.9	161.9	96.6	122.8	12.6
8.5	1370	88:48	87.9	159.1	96.6	118.8	12.6
86	1387	88:43	87.7	156.0	96.6	114.6	12.6
DA#35	1393						
87	1403	88:50	87.7	161.6	96.6	115.5	12.6
			0.7. 4	158.6	96.6	111.8	12.6
88	1419	88:45	07.4	1.20.0	20.0	111.0	1 2
88 89	1419 1435	88:40	87.4 87.1	155.5	96.6	108.1	12.6

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HX FOP SECONT

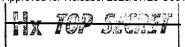
BIF-007/D-0017-75

TABLE I - | Cont'd,

BASIC ORBITAL PARAMETERS

DAY	REV	PERIOD	PERIGEE	APOGEE	INC.	ARG/PER	B ANG
OA#37	1443						
90	1451	88:55	88.2	157.7	96.6	137.9	12.6
91	1468	88:50	88.4	154.7	96.6	133.2	12.6
92	1484	88:45	88.2	152.0	96.6	129.0	12.6
0A#38	1490						
93	1500	88:50	87.8	157.9	96.6	127.7	12.6
94	1516	88:46	87.7	155.2	96.6	123.7	12.6
95	1533	88:40	87.5	152.1	96.6	119.8	12.6
OA#39	1538						
96	1549	88:51	88.0	160.1	96.6	123.4	12.6
97	1565	88:46	87.7	156.9	96.6	119.5	12.6
98	1581	88:41	87.4	153.6	96.6	115.6	12.6
OA#40	1587						
99	1597	88:53	87.9	162.8	96.6	119.5	12.5
100	1614	88:47	87.6	159.4	96.6	115.4	12.5
101	1630	88:42	87.2	156.1	96.6	111.5	12.5
OA#41	1636						
102	1646	88:51	88.6	162.1	96.6	115.9	12.4
103	1662	88:46	88.3	158.9	96.6	112.2	12.4
104	1578	88:41	87.9	155.5	96.6	108.5	12.3
OA#42	1684						
105	1695	88:52	88.7	163.0	96.6	112.3	12.3
106	1711	88:46	88.2	159.3	96.6	108.6	12.2
107	1727	88:40	87.5	155.0	96.6	105.1	12.2
OA#43	1733						
OA#44	1735						
108	1743	88:54	89.0	156.4	96.6	137.7	12.1
109	1759	88:49	88.9	153.6	96.6	133,4	12.0
110	1776	88:43	88.7	150.4	96.6	128.6	12.0
OA#45	1782						
111	1792	88:50	89.1	155.3	96.6	131.1	11.9
112	1808	88:45	88.8	152.4	96.6	127.3	11.8
113	1824	88:40	88.6	149.3	96.6	123.3	11.8
OA#46	1830						
114	1841	88:52	89.0	157.9	96.6	127.9	11.7
. 115	1857	88:48	88.9	155.4	96.6	123.9	11.6
116	1873	88:43	88.7	152.5	96.6	119.9	11.5
OA#47	1879						
117	1889	88:52	89.0	160.1	96.6	122.5	11.4
118	1906	88:47	88.8	156.7	96.6	118.3	11.3
119	1922	88:41	88.3	153.5	96.6	114.4	11.2
OA#48	1928	0.0 - 50	0.0	io) e	000	4 611	1.1
120	1938	88:52	88.8	161.5	96.6	118.0	11.1
121	1954	88:47	88.6	158.5	96.6	114.2	11.0
122	1970	88:42	88.3	155.5	96.6	110.5	10.9

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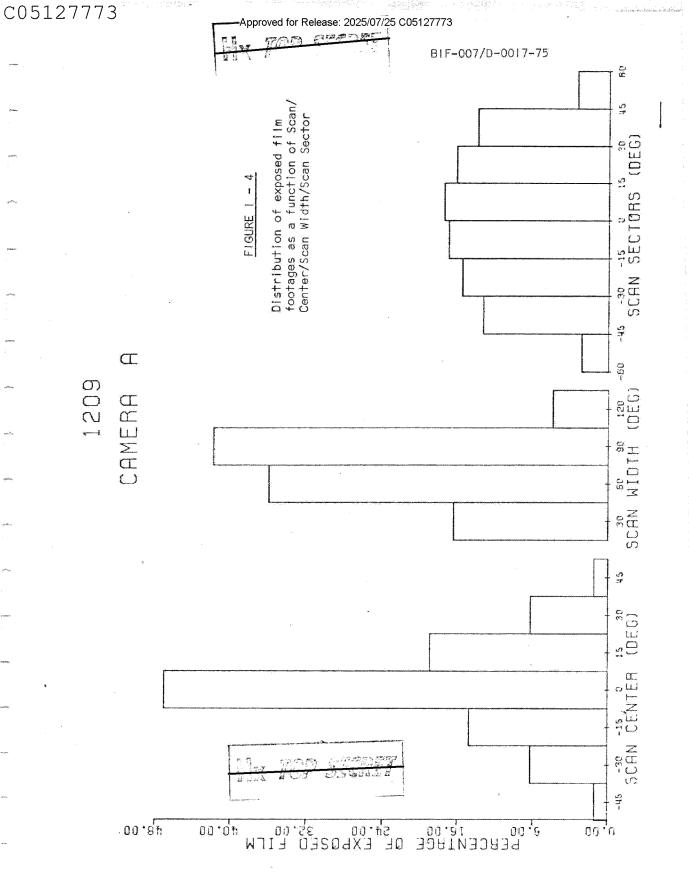


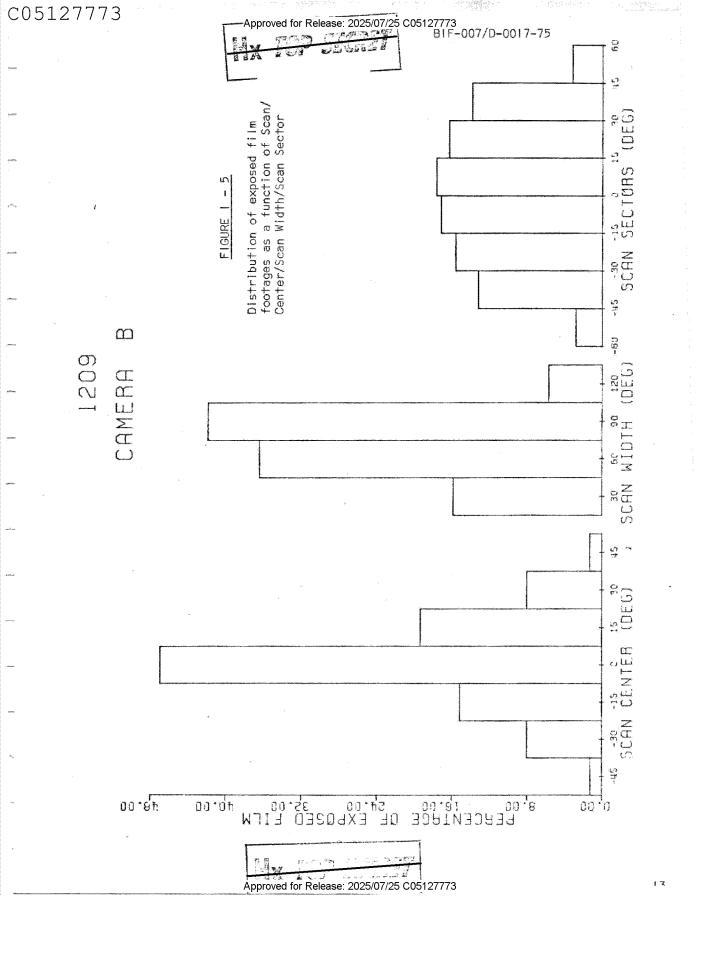
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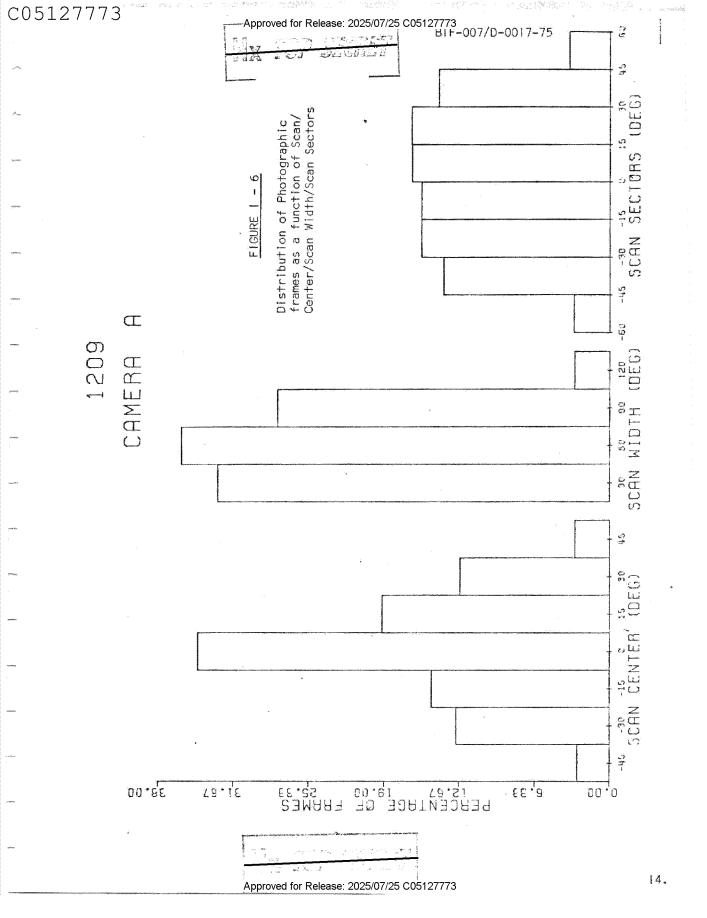
TABLE 1 - 1 Cont'd.

BASIC ORBITAL PARAMETERS

DAY	REV	PERIOD	PERIGEE	APOGEE	INC.	ARG/PER	B ANG
OA#49	1976			,			
123	1987	88:53	88.8	164.0	96.6	113.2	10,8
124	2003	88:48	88.4	160.7	96.6	109.4	10.7
125	2019	88:43	88.0	157.1	96.6	105.9	10.6
OA#50	2025		20				
126	2035	88:52	88.8	163.9	96.6	108.9	10.4
127	2051	88:46	88.5	160.6	96.6	105.4	10.3
128	2068	88:40	87.8	155.9	96.6	101.4	10.2
OA#51	2074						
129	2084	88:51	88.5	164.3	96.6	105.3	10.1







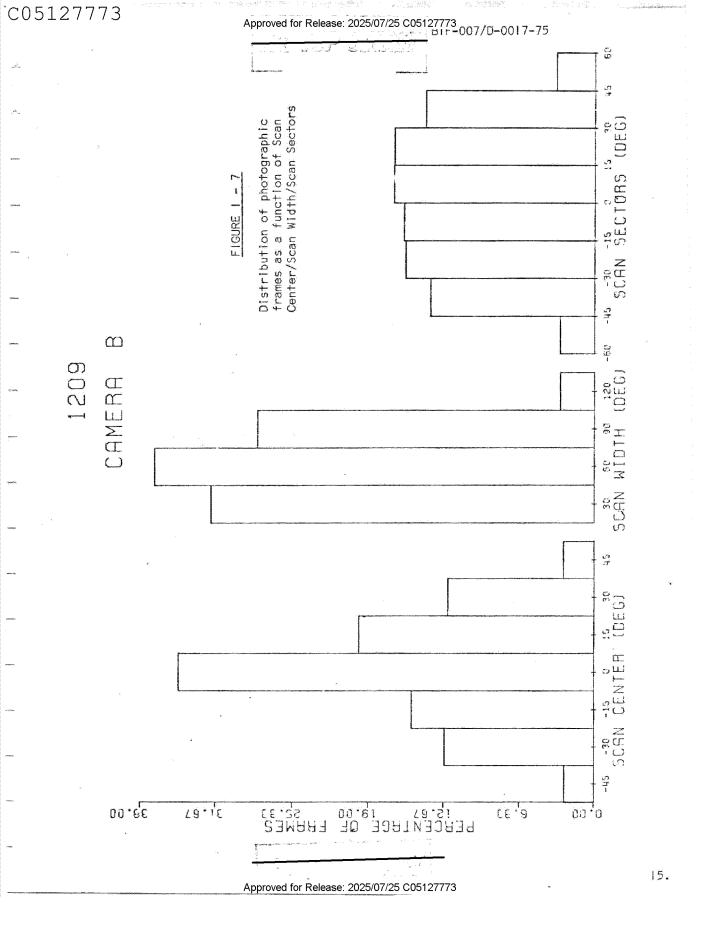


FIGURE 1 - 8

Distribution of land mass coverage as a function of Scan Sectors

1209

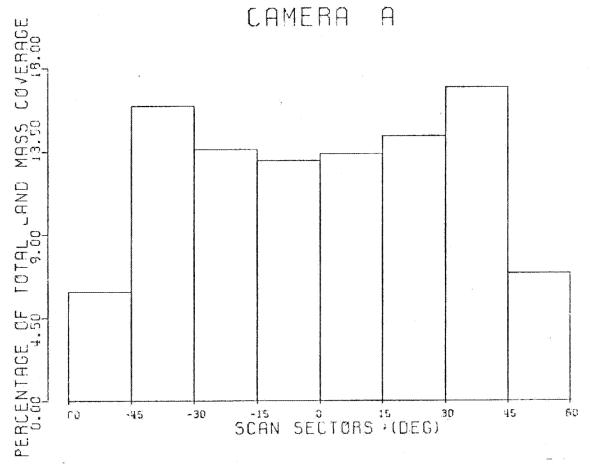
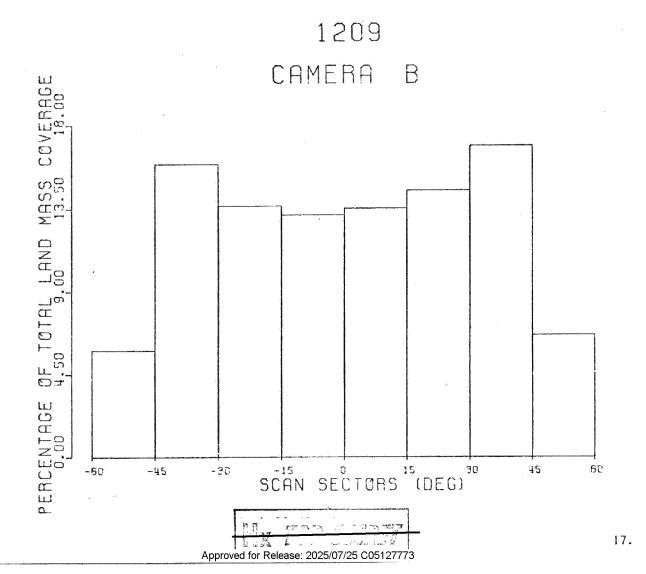
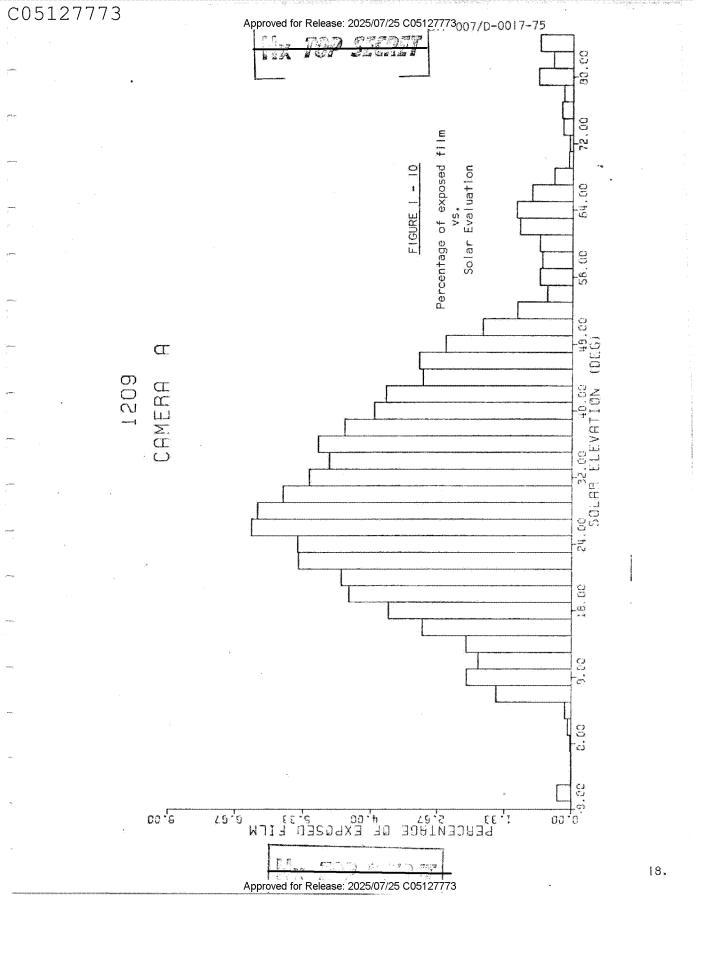


FIGURE I - 9

Distribution of land mass coverage as a function of Scan Sectors



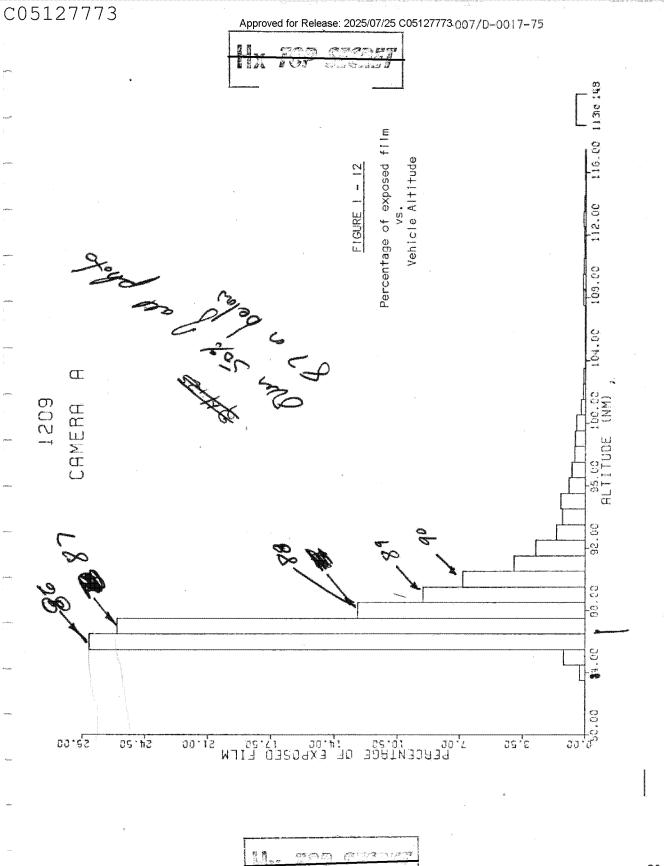


00.00 00.00 00.00

PERCENTAGE 1, 33 EE, 1

OF EXPOSED 5,33

00 5



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FIGURE 1 - 14

Percentage of exposed film vs.
Latitude

Between 30 - 50 118 115 118 118

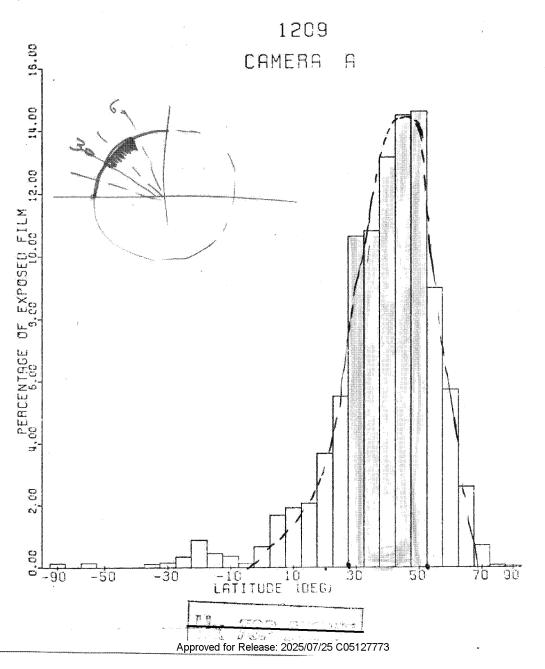
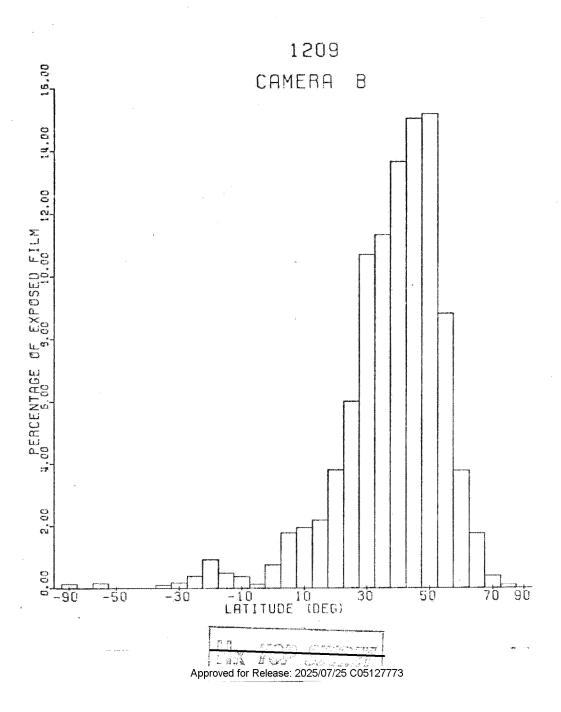


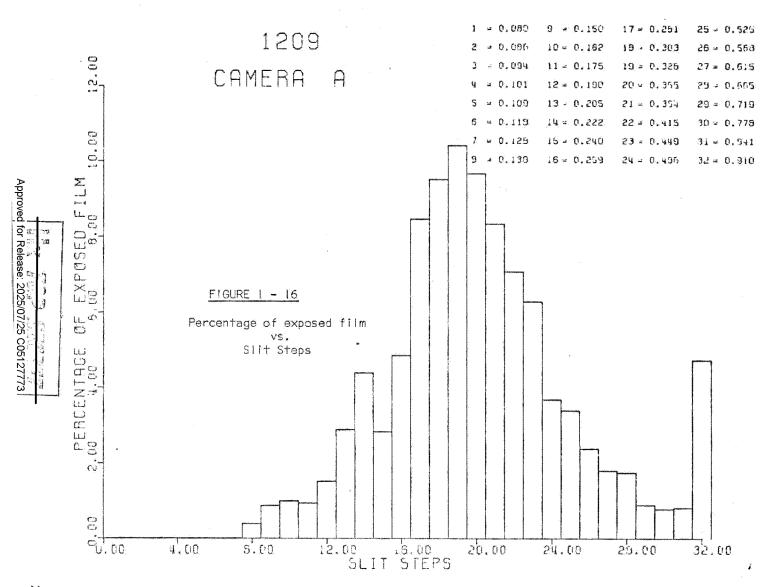
FIGURE 1 - 15

Percentage of exposed film vs. Latitude

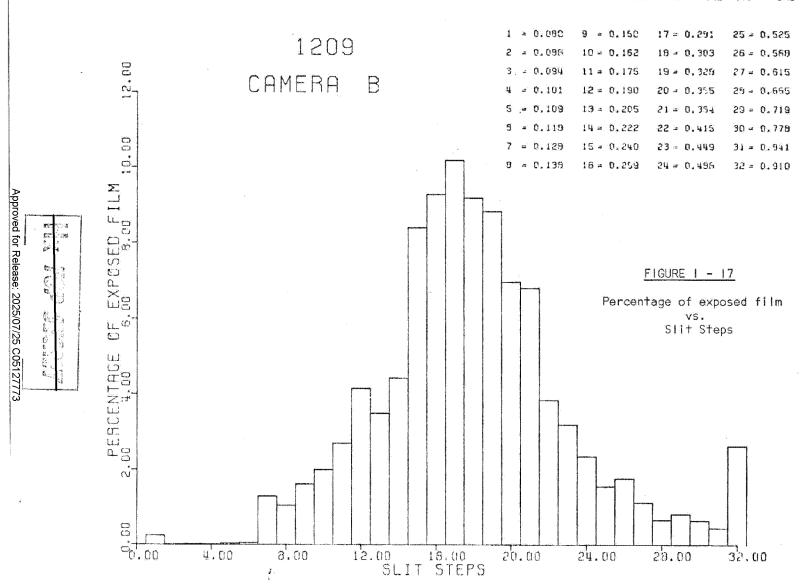


STEP & CAL STEP - CAL STEP - CAL STEP - CAL





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FIGURE 1 - 18

Distribution of fully framed Targets vs. Scan Sectors

1209 CAMERA A

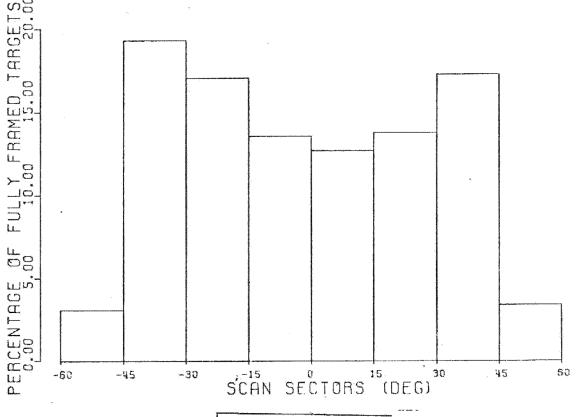
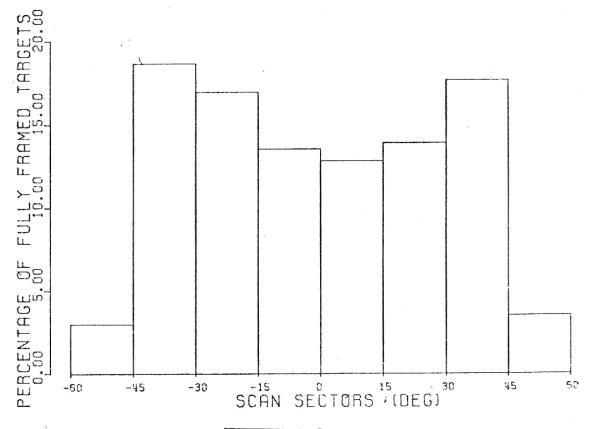


FIGURE 1 - 19

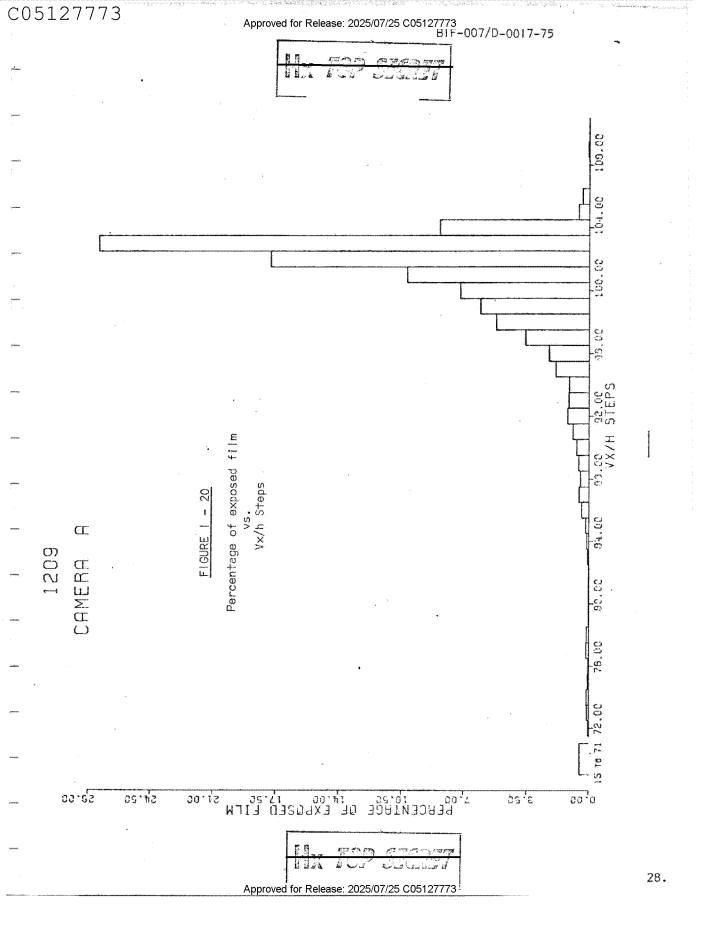
Distribution of fully framed Targets vs. Scan Centers

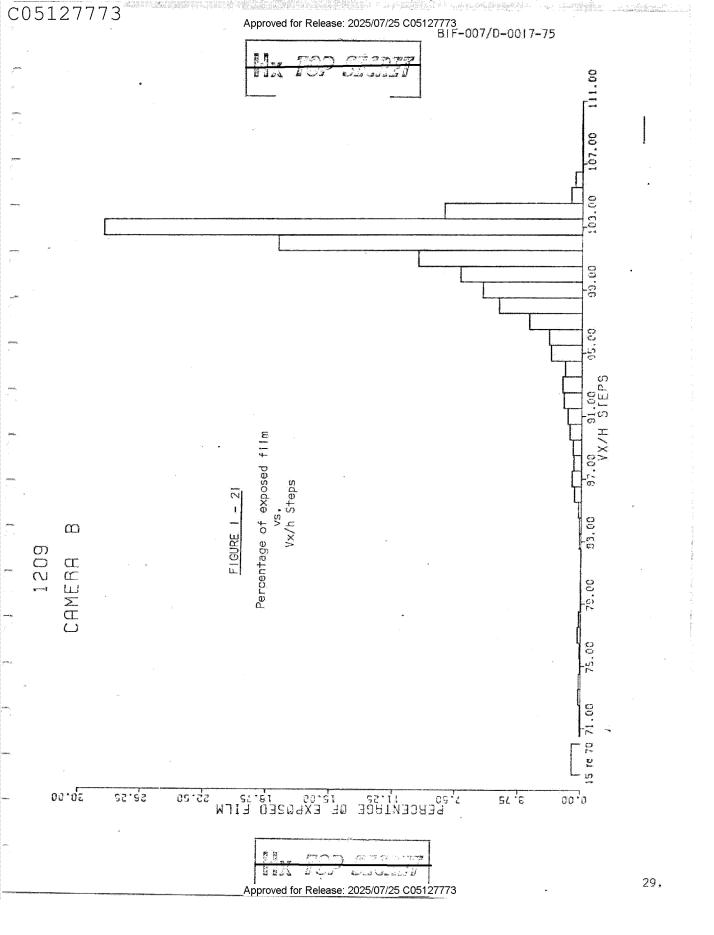
1209 CAMERA B

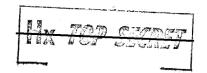


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27.







2.0 SENSOR SYSTEM PERFORMANCE

2.1 Coarse Film Path

The coarse film path, consisting of the supply, looper, steerers and take-ups of both cameras exhibited characteristic performance throughout the mission.

2.1.1 Film Path Tracking

The system was operated with a maximum rewind of 5 ips, and no constraint on scan center or scan angle for this mission.

Both take-ups were stacked properly throughout the mission. Film stacks were well-centered on the take-up core and there was no evidence of mistracking.

2.1.2 Aft Camera Supply Depletion

On Rev 2086, Mission Op 757, during frame 10 of a planned 13 frame operation, the Aft Camera supply was depleted and loss of tension in the film path initiated an emergency shutdown.

2.1.3 Forward Camera Supply Depletion

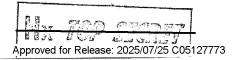
On Rev 2090, Mission Op 759, during frame 16 of a planned 16 frame operation, the Forward Camera supply was depleted and loss of tension in the film path initiated an emergency shutdown.

2.1.4 Constant Velocity to Refrieve Film Tail

On Rev 2092, as part of the recovery prep sequence, a constant velocity was run with the emergency shutdown overridden to pull the remaining film forward into the take-up.

2.2 Fine Film Path

Fine film path diagnostics indicated proper hardware performance throughout the mission for both camera systems.





2.2 Fine Film Path-Cont'd.

2.2.1 Fine Film Path Tracking

Both cameras tracked the film nominally for all scan lengths and scan centers throughout the mission. The Forward Camera tracking did not change from pre-launch, while the Aft Camera experienced an 0.8 mm mean tracking shift downward from pre-launch tracking.

2.3 Command and Control

The sensor system performance with respect to the Command and Control Subsystem was nominal throughout the mission. All commands were properly received and executed.

2.4 Sensor System Control

The Sensor System Control was accomplished throughout the mission on SCCI without anomalies or failures.

2.5 Optical Bar Performance

The Optical Bars performed properly throughout the mission. Variations between commanded and actual OB velocities were no different than those noted during pre-flight system test and were within the specification limits of .00054 rad/sec.

2.6 LSFS/Focus

The LSFS output, as with previous Sensor Systems, was deemed reliable only on the first operation of each day (i.e., after three hours of non-operation and during the first five minutes of the first subsequent operation). Readings of the LSFS output were taken only at these times throughout mission 1209.

Pre-flight determined focus settings were:

31 microns for 1414 film on the Forward Camera; 70 microns for 1414 and 100 microns for both SO-255 and SO-130 on the Aft Camera.

2.7 Instrumentation

All instrumentation operated normally throughout the mission. The system provided consistent and accurate data for analysis and verification of camera status.

However, one segment of the instrumentation and data system, the strip charts, indicated that the Aft system's drive Sum Error signals appeared to have a peculiar high amplitude and



2.7 Instrumentation - Cont'd.

low frequency oscillation from FT+ to the beginning of the 'P' mode when processed in format 'C' but not in format 'B'.

The explanation for this peculiarity is that the Aft system has an inherent 23 H_Z harmonic frequency which was beating against the format 'C's 25 samples/second sampling rate as opposed against format 'B's 500 sps rate, thus creating a 2 H_Z wave signal which was superimposed upon the existing Drive Sum Error trace.

Also it was reported by the P.I.'s, after reviewing the material from TU3, that the dimension from start of OP mark-to-start of first frame on the Forward system, had decreased to approximately 3.5 to 4 Inches from the normally observed value of 4 to 4.5 inches. This decrease was originally thought to be an early indication of possible problems in the SCC. However, It appears that something; e.g. spring constants, emulsion, particles, had changed the shutter's mechanical delay mechanism.

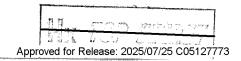
As this dimensional decrease corresponds to the minimum granularity of the shutter open/close indicator in mode 122, it confirms the contention that this problem could not have been detected by utilizing the instrumentation data but only by visually inspecting the material.

2.8 Pneumatics

The pneumatic system nitrogen reserve status for mission 1209 was as follows:

		TANK	4	TANK B Total					
<u>Event</u>	Press. (psi)	Temp	Mass (1bs)	Press (psi)	Temp (Of)	Mass (1bs)	Mass (lbs)		
Liftoff	3332	75	17.33	3332	75	17.33	34.8		
End of Primary Mission	112	71	0.63	140	71	0.78	1.4		

The computed PN+ use rate was a constant 0.023 lbs/min. From the outset of the mission a statistical trand analysis was maintained to correlate use rate in terms of expended nitrogen mass per foot of spooled take-up film versus remaining supply unit film and





nitrogen reserve. The analysis, presented in both graphical and tabular form, served the purpose of managing camera operation parameter (scan length, scan center, frame count) to preclude depletion of the nitrogen reserve prior to complete utilization of the SV film load.

In addition to the normal D bar use requirement, it was occassionally necessary to acuate the pneumatic system operate valves to maintain the film path pressure above the ballooning criterion. The initial repressurization occurred after transfer to TU-4 and was repeated as required for the remainder of the mission. Although the path leak rate was within specification requirements, the combination of decreased volume and short operations with corresponding small increases in path pressure, separated by long quiescent periods caused the repeated occurrence of the low pressure condition. To minimize the additional gas usage, a procedure was used wherein the path was repressurized, increased by approximately 0.1 psi, only at those times the pressure had decayed to the ballooning limit.

2.9 Trend Analysis

A statistical trend analysis of sensor system performance was maintained by the Systems Integration Section throughout Mission 1209. Data samples were taken from one operation per day, when available, and mean values and standard deviations were calculated and plotted for selected functions to facilitate the detection of any long term trends that would indicate the onset of system degradation. The functional parameters used for the analysis were as follows:

- Film to Bar Sync Velocity Error (P451, P452)
- 2. Metering Capstan Summed Error (403, P404)
- 3. Platen Skew Error (P415, P416)
- 4. Platen Photo Summer Error (P4)1, P412)
- 5. Input Drive Capstan Summed Error (P803, P804)
- 6. Output Drive Capstan Summed Error (P811, P812)
- 7. Supply Drive Summed Error (P105, P106)
- 8. Take-up in Use Drive Summed Error (TSEA, TSEB)
- 9. Optical Bar Summed Error (P501, P502)
- 10. OB Velocity Error
- II. Looper Position (P601, P602)
- 12. Film Path Carriage Position (P713, P714)
- 13. Take-up Carriage Position (P951, P952)



2.9 Trend Analysis-Cont'd.

System performance was normal throughout the mission. However, small shifts were evident in certain parameters and are summarized as follows:

- IDC-B & ODC-B The 2 Sigma deviation improved slightly after transfer from TU-1 to TU-2.
- <u>TU-B Steerer Position</u> The mean position gradually shifted from approximately +0.01 inches to -0.015 inches after transfer to TU-3.



3.0 MISSION EVENT HISTORY

A summary listing of all sensor system photographic operations is presented in Appendix A-I of this report. The summary primarily covers operational photography, but also includes SS and PFA engineering photography. The following is a chronological description of these engineering operations plus other special events that occurred during Mission 1209.

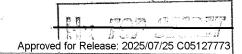
3.1 Ascent

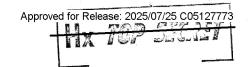
The countdown and launch were accomplished without incident, with uncage (sequences 204 and 205) and OB stow (sequences 213 and 214) occurring in a normal manner following BV-SV separation. These events were verified from tape recorder playback at Rev I POGO.

3.2 Health Checks

Day I operations through Rev 4 were designed to verify system health and confirm orbit operational readiness. An engineering operation designed as a baseline test was performed on Rev 8. The health check events were as follows:

- Rev I: An uncage verification check, sequence 215, was performed over POGO to confirm the uncage event.
- Rev 2: A constant velocity run, sequence 208, was performed over KODI. This was the first attempt to transport film after launch. The sensor system worked properly, and the film was correctly aligned within the film path. Steerers, tensions, and take-up and supply drive summed errors were well within limits.
- Rev 4: The sensor system health check, sequence 175, was performed over POGO. All sensor system executed commands were functionally verified, including all tested bits of the variable commands. Focal plane position indicated 31 microns for the Forward camera, and 70 microns for the Aft camera.
- Rev 8: A scheduled engineering operation, sequence 209, was performed over COOK to provide characteristic telemetry data for comparison with data from any future identical functional check. In the event of an anomaly, the telemetry signatures of the two runs could then be equated and any suspected system degradation determined.





3.3 MISSION 1209 ENGINEERING

		TÉST TYPE	DBJECTIVE
	1	1414 THRU FOCUS	OPTIMIZE FOCUS SETTINGS. COMPLETED IN RV-1.
	ЗЯ		DETERMINE OPTIMUM SKEW ANGLE AND FILM VELOCITY OOAA SETTINGS. COMPLETED IN RV-2.
1	48	\$0255 RADIOMETRIC CAL	DETERMINE IMAGE TRANSFER AND RADIOMETRIC CALIBRATION. COMPLETED IN RV-2.
	48	SO255 TONE REPRODUCTION	DETERMINE TONE REPRODUCTION. COMPLETED IN RV-2.
	4C	SO255 PROCESSING STUDIES	DETERMINE PROCESSING STUDIES. COMPLETED IN RV-2.
	5	SG-130 RADIOMETRIC CAL	DUPE TONE REPRODUCTION AND RADIOMETRIC CALIBRATION. COMPLETED IN RV-3.
	7	TUCSON ACQUISITION	STANDARD SCENE FOR MISSION TO MISSION QUALITY COMPARISON. COMPLETED IN RV-1,2 AND 4.
	8	SO255 THRU FOCUS	OPTIMIZE FOCUS SETTINGS. TEST CANCELLED IN RV-1.
	9	TRI-BARS FOR RESOLUTION	PHOTO QUALITY ASSESSMENT. COMPLETED IN RV-1,2,3 AND 4.
	10		ASSESS SMEAR AS A FUNCTION OF SCAN ANGLE. COMPLETED IN RV-4.
	12		PHOTO/EM CORRELATION. COMPLETED IN RV-1,3 AND 4.
	13	STELLAR PHOTOGRAPHY	EVALUATE CAPABILITY OF ACQUIRING STELLAR IMAGES. COMPLETED IN RV-4.
	14	1414 SPECIAL TARGETS	ASSESS PHOTO QUALITY. COMPLETED IN RV-4.
	15		EVALUATE DOUBLE ANNULUS TARGET FOR FOCUS/SMEAR DETERMINATION. COMPLETED IN RV-4.

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3.4 MISSION 1209-1	SPECIAL	EVENTS
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	Se a r	1,12222			- AT			
		REV	OPN	TEST	PRE WX	EVENT/LOCATION	WX WX	FTG
						PREFLIGHT FOOTAGE TUA PREFLIGHT FOOTAGE TUB		1601 1609
		0.8				UNCAGE/SCC 1 SELECT		
		0.8				STOW A/STOW B		
		1				UNCAGE VERIFY		
		2				UNINHIBITED CY		102
	,	4	1-3			SS HEALTH CHECK		188
		8	7			SS ENGINEERING TEST		63
		65	37	1	95	1414 THRU FOCUS SAN FRANCISCO 10/0/-10	99	41
		167			>	PM EQUALIZATION		
		177	93	-	98 95	1414 THRU FOCUS MILWAUKEE –10/0 CHICAGO 10/20	20 20	54
		178	94	1	75	1414 THRU FOCUS PHOENIX 6/0	99	28
		226	111	1	99	1414 THRU FOCUS DALLAS/FT WORTH -10/0	29	31
		248	119	age of the state o	65	1414 THRU FOCUS KOBE/OSAKA 20/10	ing seci Sec and	45
		259	122	7,9 15	80	1414 QUALITY STANDARD TUCSON W∕5T,DA	65	29
×		264	123	Animode	65	1414 THRU FOCUS TOKYO -20/-10	95	36
		276	127	1	65	1414 THRU FOCUS VANCOUVER 20/0	0 0	29



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*	3.4	MISSIO	N 120	9-1 SPE	CIAL	EVENTS CONT'D		
		REV	DPH	TEST	PRE WX	EVENT/LOCATION	VER WX	FTG
ymar 		290	133	1	95 95	1414 THRU FOCUS BALTIMORE 20/0 WASHINGTON 10/0	20 75	42
çangur		306	138	1	35	1414 THRU FOCUS NEW YORK 10/0/-10/-20	0 0	135
· period		307	139	1.	75	1414 THRU FOCUS MINNEAPOLIS 20/10	65	39
;• *******		307	140	1.	99	1414 THRU FOCUS DALLAS –20/–10 INCLUDES PROTECTIVE WRAP	80	130
AND RESIDENCE OF THE PERSON OF		308				TRANSFER TO TUZ-PREP 1		

TU FOOTAGE 2584 2592
TOTAL FOOTAGE 2584 2592

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	3.5	MISSID	Н 1209	9-2 SPE	CIAL	EVENTS		
 		REV	OPH	TEST	PRE MX	EVENT/LOCATION	VER NX	FTG
ja en		308				TRANSFER TO TUZ - PREP 1		13
		309				TU2 - PREP 2		50
Nipoleph		340	151	7,9 15	7 5	1414 QUALITY STANDARD TUCSON W∕5T,DA	95	29
-		350				1414 OOAA PSIB NOM TO -7		
	+	367				TRANSFER TO 30255		
Spirot		378	162			FIRST OPH S0255		
этнерес		388	168	4B	90	SO255 TONE REPRODUCTION KANSAS CITY	99	29
-audiony		405	173 174	40	90 90	SO255 PROCESSING STUDIES OGDEN/SALT LAKE -1/3,NOM PHOENIX -1	99 99	68
		421	180	40	99	SO255 PROCESSING STUDIES ALBUQUERQUE -2/3	99	28
,		434				TRANSFER TO 1414		
		435	184			FIRST OPN 1414		
		438	185	10	90	1414 SMEAR VS SCAN SAN FRANCISCO +SECTOR	90	37
junci		486	* 201	15 14	90	1414 SPECIAL TARGET TUCSON W/DM STATIC DISP	99	29
Nadistra -		519	212	38	35	1414 SMEAR SLITS SAN FRANCISCO BAY AREA	50	36
		534	217	ЗН	85	1414 SMEAR SLITS DALLAS/FT WORTH	99	35
		566	227	3 A	75	1414 SMEAR SLITS DETROIT	90	35

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	3.5	MISSID	N 1209	9-2 SPE	CIAL	EVENTS CONT'D		
The state of the s		REV	OPN	TEST	PRE WX	EVENT/LOCATION	NEK NEK	FTG
- Section		582	240	3 A	80	1414 SMEAR SLITS TAMPA/ST PETERSBURG	99	35
		605	254			PN EQUALIZATION	%	
		616	257	ЗЯ	95	1414 SMEAR SLITS SAN DIEGO	99	31
		681	280	38	90	1414 SMEAR SLITS LOS ANGELES	99	34
-		754		(TRANSFER TO S0255		
		754	314			FIRST OPN SÓ255		
		777	323	4B	90	SO255 TONE REPRODUCTION BATON ROUGE	99	32
		778	324	4H	99	SO255 RADIOMETRIC CAL PHOENIX	Sing (m)	27
ára.		794	331	48	90	SO255 TONE REPRODUCTION ALBUQUERQUE		28
merç.		817	343			PN EQUÂLIZATION		
		819				TRANSFER TO 1414		
		819	346			FIRST OPH 1414		
_		886	366			PROTECTIVE WRAP		150

TU FOOTAGE 726 726
TOTAL FOOTAGE 3310 3318

TRANSFER TO TUB-PREP 1

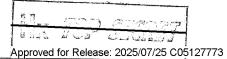
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3.6 MISSION 1209-3 SPECIAL EVENTS

REV	OPN	TEST	PRE WX	EVENT/LOCATION	VER NX	FTG
890				TRANSFER TO TUS-PREP 1		13
891				TU3 - PREP 2		50
960				PATH PRESSURIZATION		
979				1414 OOAA PSIA NOM TO -2		
1054	421	12	80	1414 QUALITY VARIABILITY LOS ANGELES	90	36
1127				TRANSFER TO SO255		
1129	458			FIRST OPN S0255		
1180				TRANSFER TO 1414		
1189	472			FIRST OPN 1414		
1223	490			PN EQUALIZATION		
1247	501	10	75	1414 SMEAR VS SCAN ATLANTA -SECTOR	99	29
1265	508	10	55	1414 SMEAR VS SCAN SAN FRANCISCO —SECTOR	95	.34
1275				TRANSFER TO SO-130		
1275	514			FIRST OPN SO-130		
1297	521	gree- June - " cua	90	SO-130 RADIOMETRIC CAL PHOENIX	85	29
1313	527	lon.	95	30-130 RADIGMETRIC CAL ALBUQUERQUE	95	29



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3.6 MISSION	1209-3	SPECIAL	EVENTS	CONT'I
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REV	OPH	TEST	PRE WX	EVENT/LOCATION	VER WX	FTG
1320	530			TRANSFER TO 1414		
1321	531			FIRST OPH 1414		
1345	541	12	90	1414 QUALITY VARIABILITY DALLAS/FT WORTH	99	32
1356	550			PROTECTIVE WRAP		289
1360				TRANSFER TO TU4-PREP 1		

TU FOOTAGE 541 541
TOTAL FOOTAGE 3851 3859

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3.7 MISSION	1209-4	SPECIAL	EVENTS
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REV	OPN	TEST	PRE WX	EVENT/LOCATION	VER WX	FTG
1360			*.	TRANSFER TO TU4-PREP 1		13
1361			T.	TU4 - PREP 2		50
1377				PATH PRESSURIZATION		
1378	552	7.9 15	99	1414 SPECIAL TARGET TUCSON W/DA	99	29
1385				PATH PRESSURIZATION		
1392				PATH PRESSURIZATION		
1400				PATH PRESSURIZATION		
1411	560	A Com	90	1414 QUALITY VÄRIABILITY SAN FRANCISCO	99	37
1426	568	10	99	1414 SMEAR VS SCAN DALLAS/FT WORTH -SECTOR	99	31
1427	569	14	99	1414 SPECIAL TARGET BARSTOW MCSC,DA	99	28
1476	589	10	70	1414 SMEAR VS SCAN SAN FRANCISCO +SECTOR	70	34
1555	631	14 15	65	1414 SPECIAL TARGET CAPE CANAVERAL W/DA	60	29
1571	640	10	80	1414 SMEAR VS SCAN NEW YORK -SECTOR	99	38
1621	667			PN EQUALIZATION		
1637	675	10	99	1414 SMEAR VS SCAN DALLAS/FT WORTH +SECTOR	99	36
1725				PN EQUALIZATION		
1769	713	13		STELLAR PHOTOGRAPHY		153

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3.7	MISSION	1209-4	SPECIAL	EVENTS	COMTID
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REV	OFH	TEST	PRE WX	EVENT/LOCATION	VER WX	FTG
1836				PATH PRESSURIZATION		
1857				PATH PRESSURIZATION		
1836	739	10	99 99	1414 SMEAR VS SCAN BALTIMORE -SECTOR WASHINGTON -SECTOR	99 99	38
1872				PATH PRESSURIZATION		
1905				PATH PRESSURIZATION		
1969				PATH FRESSURIZATION		
1978				PATH PRESSURIZATION		4.
2010	748	10	75	1414 SMEAR VS SCAN DALLAS/FT WORTH -SECTOR	99	33
2052				PATH PRESSURIZATION		
2065		'S'		PATH PRESSURIZATION		
2079				PATH PRESSURIZATION		
2086	757			LAST AFT OP (10 FR)		
2090	759			LAST FWD OP (16 FR)		
2092				TU4-PREP 2/CV		

TU FOOTAGE 549

549

TOTAL FOOTAGE 4400

4408

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44.



3.8 Solo Phase

Solo testing on SV-9 was performed to meet three specific objectives:

- Test SS-I was designed to provide data which would determine the gas flow impedance of the Film Exit Vestibule (FEV) when a pressurized supply was exhausting to a TCA in vacuum.
- Test SS-2 was designed to confirm previously determined constraints of plus 170 microns and minus 120 microns respectively as the maximum and minimum allowable focal plane position.
- Test SS-3 was performed to provide temperature data which would allow estimation of TCA frame and midsection bending during a simulated stellar camera calibration.

3.8.1 Test SS-1

Test SS-I was performed in three separate steps. In step one, the supply was first pressurized to .73 psi. The supply was then vented to the TCA via the A-side seal door (SLDA) during a five minute Mono-A constant velocity operation.

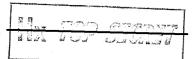
The data for this portion of the test was as follows:

Vehicle	Supply	Average	Event
Time	Pressure (psi)	Supply Temperature	
348427.0	0.73	72.5	SLDA OPEN
348728.0	0.69	72.5	SLDA CLOSE

This data established a decay rate of .000133 psi/second

In steps two and three of Test SS-I, the supply was not repressurized. Since, the B-side pneumatics tank was depleted during the supply pressurization in step I, the High Pressure Crossover Valve (HPCV) was opened for the duration of the second part of the SS-I test. This was to assure proper regulator pressure on the B-side for seal door operation.

In step two, a Mono-B constant velocity operation was performed and the supply was vented to the TCA via the B-side seal door (SLDB). The data from this operation are as follows:



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Vehicle	Supply	Average	Event
Time	Pressure (psi)	Supply Temperature	
496622.8	0.63	71.5	SLDA/B OPEN
496924.8	0.60	71.5	SLDA/B CLOSE

The data established a decay rate of .000099 psi/second.

In step three of test SS-1, the supply was vented to the TCA for twenty minutes via SLDA and SLDB during a constant velocity operation. The data was as follows:

Vehicle	Supply	Average	Event
Time	Pressure (psi)	Supply Temperature	
667054.8	.57	66/69	SLDA/B OPEN
668255.8	.43	65/69	SLDA/B CLOSE

This data established a decay rate of .000117 psi/second.

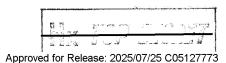
The data for parts one, two and three of test SS-I are on tracking station tapes 2113P, 2141C, and 2175H, respectively.

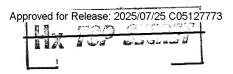
3.8.2 Test SS-2

To confirm the maximum focal plane adjustment constraint of plus 170 microns, Focal Plane A (FPA) and Focal Plane B (FPB) were retreated from the Best Plane of Focus (BPF) to the plus 170 micron constraint value. This amounted to a 140 micron retreat for FPA and a 100 micron retreat for FPB. When this was achieved, the focal planes were commanded to retreat another 40 microns in four 10 micron steps given at six second intervals. The FPA telemetry indicated a stop position of 203.1 microns with a corresponding LSFS value of 173 counts. The FPB telemetry indicated a maximum position of 210.4 microns. However, the LSFSB saturated at an indicated FPB position of 201.2 microns.

To confirm the constraint of minus 120 microns for the low end of allowable focal plane position, FPA and FPB were first commanded to advance 310 microns. They were then commanded to advance another 100 microns in 10 micron intervals. At this time the focal planes were commanded to retreat 10 microns to determine whether they had driven off the drive cam and become imoperable.

FPA telemetry indicated that the FPA stopped advancing at a position of minus 188.3 microns and that it did not respond to the final 10 microns retreat commanding.





Test SS-2 Cont'd.

FPB telemetry indicated that FPB advanced to a minus 166.1 microns before it stopped. Upon receipt of the 10 micron retreat commanding, FPB retreated, according to telemetry, to a position of minus 155.1 microns.

The LSFSA and LSFSB data indicated low saturation was reached on both systems somewhere in the region of minus 90 to minus 100 microns. Since the FP systems were still being advanced when these positions were achieved, a more precise functional limit on the minimum allowable FP position could not be ascertained.

The commanding and telemetry data are summarized in Figures 3-1 & 3-2. The telemetry data was played back at 2124C.

3.8.3 Test SS-3

Test SS-3 was performed in conjunction with Solo Test EDAP-2 (SBAC) on Rev 2186. Camera power and Optical Bars were turned on at the midpoint of the dark side orbit interval and thermal data was obtained at this time. During this period the vehicle was oriented with the plane of the TCA perpendicular to the earths gravity vector and in the direction of deep space. Vehicle time for camera power on was 739689 and for power off was 739967. The thermal data record (Mode 125) was obtained at 2189P.



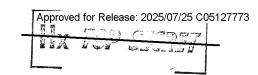
630 670 710 VEH [CApproved for Release: 2025/07/25 C05127773) 790

750

830

550

590



4.0 SENSOR SYSTEM TEST OBJECTIVES

4.1 Photographic Performance

The post flight material evaluation of mission segments 1209-1 through 1209-4 indicated the capability of the SS optical system to provide the specified photographic performance. Mission 1209 was a fall launch in early November; however, due to the active mission length of 130 days, (longest active Hexagon mission to date) the flight extended into late winter and terminated in early March.

Winter missions have characteristically lower solar elevations at the northern latitudes, snow cover and extensive ground haze. When the solar elevation becomes low, exposure times must be increased to compensate for loss of illumination. The longer exposure times thus increase the smear in the imagery. Snow cover was most prevalent at northern latitudes where the sun was lowest and the resulting shadows were longest. When the sun was very low, many targets did not receive direct lighting which lowered the contrast of the target area. Some very graphic examples of low solar elevation acquisitions were obtained during 1209-1. These acquisitions ranged from minus 0.3 degrees through plus 4.5 degrees.

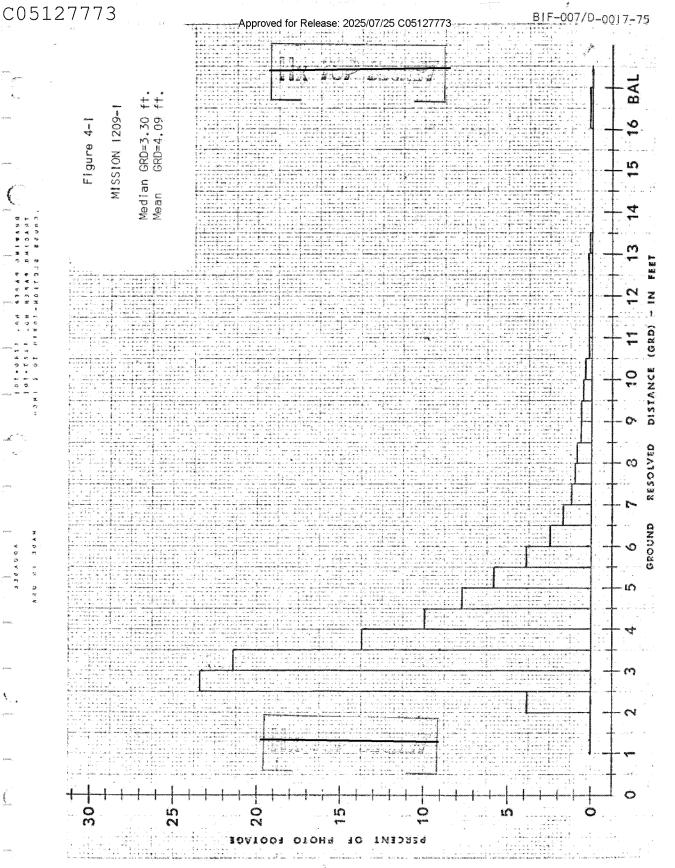
Mission segment 1209-2 contained two parts of SO-255 conventional color material. Mission segment 1209-3 contained one part of SO-255, and one part of SO-130 infrared color.

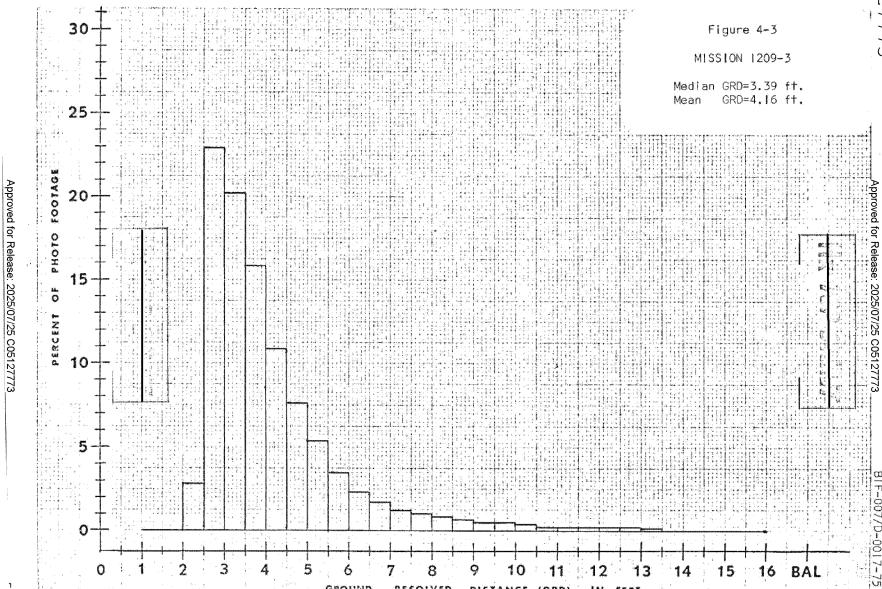
The PFA team reported that the general overall image quality of both the Forward and Aft looking cameras for the entire mission ranged from very good to poor with a consistant prefrence for the Aft camera image quality. Orbital performance prediction using CRYSPER and the actual operational parameters are included in Figures 4-1 thru 4-4 for each mission segment and Figure 4-5 for the total mission length. The discussions of image quality as a function of mission segment, which follows, is abstracted in part from the REBOUND 831 messages.

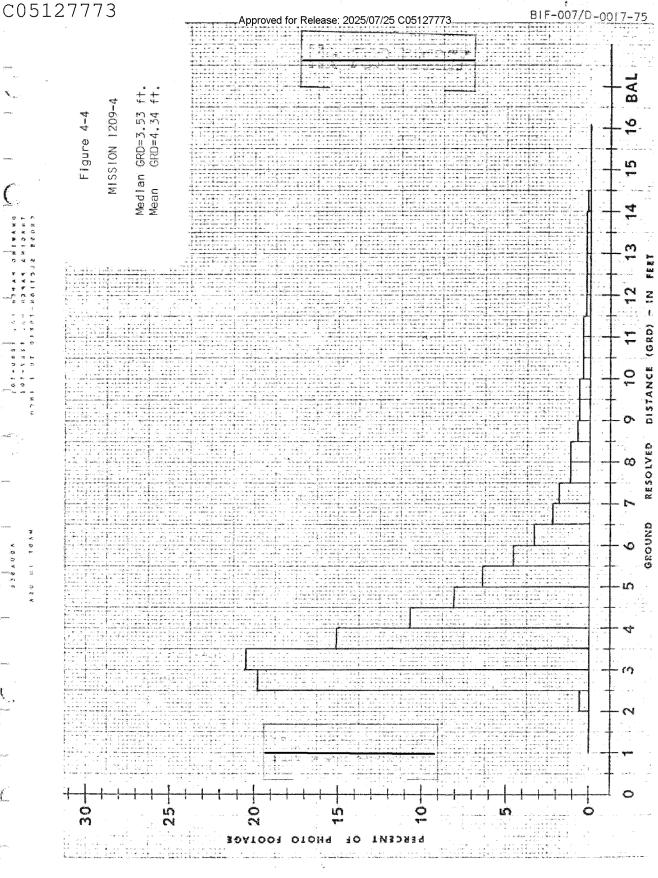
Mission Segment 1209-1

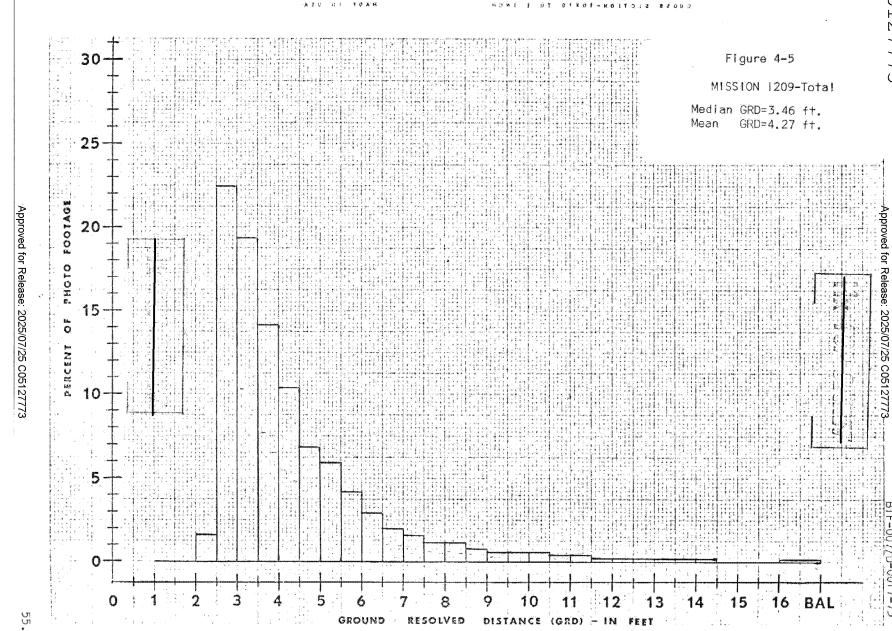
The image quality of both cameras ranged from very good to poor. Both cameras were at optimum focus. This was confirmed by both VEM and subjective analysis. The poor imagery exhibited on this mission segment was for the most part attributed to hazy or inclement weather. This imagery was characterized by a grainy

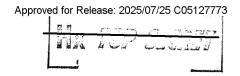












Mission Segment 1209-1 Cont'd.

appearance and poor edge definition. A majority of the 1209-1 imagery ranged from fair to good with the good quality being comparable to previous Hexagon missions. There was a definate preference for the Aft camera imagery when compared to the Forward.

During this mission segment, specific ops were acquired at very low solar elevations, and required special processing treatment. Underexposure ranged from one to eight stops. The processing chemistries utilized to gain additional film speed resulted in high base fogs of 0.50 to 0.55 density, reduced contrast and increased graininess. These parameters restricted usable magnification of this imagery to less than 30x. The image quality was generally poor.

One 51/51 tribar corn target was acquired on both the Forward and Aft cameras. The data follows:

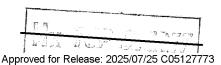
						UNADJ GRD	USTED (FT)	2: A GRD	DJUSTED (FT)
CAMERA	0P	FR	SCAN	FIELD	PLATEN	IT.	XT	JT	XT
	122 122	3	-17.8 -16.1		31 70		3.09 2.25	3.04 2.63	3.77 2.88

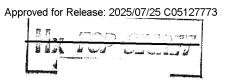
Mission Segment 1209-2

1414 Film - The image quality of both cameras ranged from very good to poor, with the majority being good. There were a few instances where the 1209-2 Aft imagery was better than the 1209-1 Aft imagery. This was attributed in part to the minus four command step change in the Aft camera in-track OOAA setting implemented on 1209-2. There was again a definite preference for the Aft camera imagery when compared to the Forward.

Eight 51/51 corn targets were acquired on the 1414 material. Six on the Forward and two on the Aft as follows:

						UNADJUSTED	2:1 ADJUSTED
						GRD (FT)	GRD (FT)
CAMERA	OP	FR	SCAN	FIELD	PLATEN	IT XT	IT XT
FWD	151	4	-11.0	-0.5	31	1.81 1.75	2,19 2.13
FWD	168	2	-15.0	-1.0	31	1.75 2.60	2.22 3.34
FWD	201	.2	+ 9.0	+1.3	31	1.72 2.25	2.11 2.76
FWD	323	3	-11.0	-0.9	31	1.85 2.36	2.28 2.92
FWD	324	4	+ 9.0	-2.5	31	2.35 2.26	2.97 2.84
FWD	331	2	+10.0	+2.4	31	1.61 2.64	1.91 3.12
AFT	151	4	-11.0	-1.7	70	1.90 2.59	2.28 2.15
AFT	201	3	+10.0	+0.5	70	1.55 1.87	1.99 2.35





 $\underline{\text{SO-255 Color}}$ - A total of 5640 feet of SO-255 was exposed in the Aft camera in two segments. The first segment was 2774 feet while the second was 2866 feet.

The image quality of the color material compared to previous color acquisitions ranged from very good to fair with most rated good. This was due in part to good weather conditions and 15 per cent cloud cover. Twenty percent of the ops exhibited very light to medium snow cover. The color balance was stightly greenish yellow for the majority of the imagery. Exposure evaluation indicated a slight bias towards under exposure of one third to one half stop. A three count (0.10 log E) exposure increase was recommended for the balance of the SO-255.

Four 51/51 corn tribar targets were acquired on SO-255.

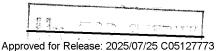
CAMERA	OP	FR	SCAN	FIELD	PLATEN	UNAD. GRD	JUSTED (FT)
CAMILIVA	<u>Ul</u>	1 13	SUM	1 L.L.L	1. LAILIN		
AFT AFT AFT AFT	168 323 324 331	2 3 4 3	-15.0 -11.0 + 9.0 +10.0	-1.5 -1.7 -0.9 +0.2	100 100 100 100	3.41 3.49 2.83 3.10	3.91 4.11 3.17 2.83

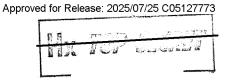
Mission Segment 1209-3

1414 Film - The overall image quality ranged from very good to poor, with the majority rated as fair. The quality was considered comparable to previous winter missions flown during late December and early January. The very good imagery was limited to the Aft camera, while the Forward camera imagery was rated from fair to good. The poor imagery was attributed to haze, snow cover, weather and low solar elevation acquisitions. This imagery was characterized by an overall grainy appearance, poor edge sharpness, and lack of contrast. The best imagery of 1209-3 was comparable to the best of 1209-2.

Six 51/51 corn tribar targets were acquired on 1414, four on the Forward camera and two on the Aft. The data is as follows:

×						UNADJ GRD	USTED (FT)		DJUSTED (FT)
CAMERA	OP	FR	SCAN	FIELD	PLATEN	IT.	XT	<u>IT</u>	XT
FWD	507	4	+3.0	-1.5	31	1.92	2.08	2.24	2.44
FWD	507	4	+3.0	-1.5	31	1.80	1.75	2.26	2.20
FWD	521	.3	-9.0	-1.5	31	2.25	2.25	2.82	2.82
FWD	527	3	+7.5	-1.2	31	2.00	2.17	2.51	2.72
AFT	507	4	+4.0	-1.2	70	1.64	2.52	2.06	3.20
AFT	507	4	+4.0	-1.2	70	1.75	2.26	2.09	3.16





SO-255 Color

A total of 2508 feet of SO-255 color film was included in the Aft camera. The quality of the color photography ranged from good to poor with the majority rated as fair. The poor imagery was affected by the same conditions as that of the 1414 acquisitions. Sixty percent of the color ops had snow cover ranging from very light to medium. The color balance was slightly greenish yellow. Examination of the SO-255 indicated generally good exposure effected by the three count (.10 log E) exposure increase implemented for 1209-3.

SO-130 Infrared Color

The Aft camera exposed 3384 feet of SO-130 infrared color in this mission segment. Overall, the image quality was good compared to previous SO-130 acquisitions, and is the best IR photography to date. The ground resolution, however, is still significantly lower than the 1414 acquisitions. The color balance exhibited a slight cyan cast. Subjective analysis indicated satisfactory exposure.

Two 51/51 corn tribar targets were acquired on the 80-130 material on the Aft camera. The data is as follows:

						UNADJ GRD	
CAMERA	OP.	FR	SCAN	FIELD	PLATEN	IT	XT
AFT AFT	521 527	3 3	-8.0 +7.5	-1.0 -1.7	100 100		5.73 5.66

Mission Segment 1209-4

The overall image quality of both cameras ranged from good to poor with the majority rated as fair. The poor imagery was characterized by an overall grainy appearance, poor edge sharpness and overall lack of crispness. Subjective comparisons of image quality between the Forward and Aft cameras indicate a continued preference for the Aft camera imagery in that it is sharper and renders fine detail somewhat better.

Subjective comparisons of the best photography of 1209-3 with 1209-4 indicated a slight decrease in image quality on the Aft camera of 1209-4. This slight decrease in image quality was attributed to haze, a significant increase in snow cover, a greater number of low solar elevation acquisitions, and a slight increase in the percent of film exposed at poorer scale. There



58.

Mission Segment 1209-4 Cont'd.

were 90 operations requiring exposure biases for snow on 1209-4 versus 46 operations on 1209-3. The percent of film exposed below 30 degrees solar elevation increased from 61 percent in 1209-3 to 67 percent in 1209-4. VEM analysis did not indicate any change in the Aft camera performance between 1209-3 and 1209-4.

Six 51/51 corn tribar targets were acquired on 1414 film; three on the Forward camera and three on the Aft.

						UNADJU GRD (STED FT)	2:1 A GRD	DJUSTED (FT)
CAMERA	OP	FR	SCAN	FIELD	PLATEN	IT	XT	IT	(FT)
FWD	552	3	-14.1	-0.6	31	1.94	2.32	2.25	2.69
FWD	569	3	+13.6	-1.2	31	1.75	2.00	1.92	2.18
FWD	631	2	-13.8	-1.2	70	2.00	1.87	2.76	2.58
AFT	552	3	-13.3	-2.1	70	2.32	3.00	2.59	3.38
AFT	569	3	+14.4	-2.2	70	2.00	2.75	2.28	3.15
AFT	631	2	-13.0	-1.3	70	1.94	2.33	2.56	3.11

Subjective analysis on 1209-4 led to the conclusion that good exposure had been maintained. Evaluation of snow surround imagery indicated that the two step snow bias performed as anticipated.

4.2 Take-Up Survival Through Recovery

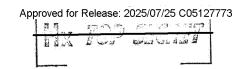
All the RV/TU assemblies arrived at the processing facility in good condition, thereby demonstrating that these assemblies maintained light tight integrity during orbital speration, re-entry, recovery and transportation to the processing site.

The core locking pins were engaged and intact in TU's 1209-1, 3 and 4. In TU 1209-2 both core locking pins were sheared and 250 feet of Forward and 350 feet of Aft film was spilled. The film was well stacked and centered on all TU's. TU 1209-4 had 50 feet off-spooled into the dome on the Forward stack. Small amounts of particulates were found in 1209-1, 2 and 3 canisters.

Related discussion of de-filming for each segment of the mission follows.



59.



4.2 Take-Up Survival Through Recovery-Cont'd.

Mission Segment 1209-1

The RV/TU arrived at the processing site in good condition on 18 November 1974.

Both stacks were well centered on the TU core and there was no evidence of mistracking. Both core-locking pins were engaged and not sheared, with no difficulty encountered in retracting.

A small amount of particulate was collected from inside the dome, but in general there was less contamination than found in previous missions.

Mission Segment 1209-2

The RV/TU arrived at the processing facility on 24 December 1974 in good condition.

The core locking pins were both sheared, resulting in film spills of approximately 250 feet on the Forward and 350 feet on the Aft, causing some wrinkling and folding. The Aft side was most severely damaged from film wedged under the builder roller. The film was found to be well centered with no evidence of mistracking.

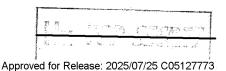
A small amount of contamination consisting of very small pieces of verious materials were found in the RV cannister. This material was collected and sent for analysis.

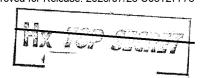
Mission Segment 1209-3

The RV/TU arrived at the processing facility in good condition on 22 January 1975.

Both core locking pins were engaged and not sheared. There was no film telescoping, spilling or despooling evident.

Three pieces of film (20, 7.5 and 2 inches long) were entrapped in the entrance cutter/sealer. A piece of white tape, 0.75 inches by I inch, was found on the Forward exit cutter blade. The canister was vacuumed and a small amount of material collected which was sent for analysis along with the tape.





4.2 Take-Up Survival Through Recovery-Cont'd.

Mission Segment 1209-4

The fourth RV/TU arrived at the processing site 8 March 1975. Both the shipping container and RV were in good condition.

Core locking pins were engaged and not sheared. Both stacks were in good condition and no telescoping observed. The outer wraps of the Forward stack, with approximately 50 feet damaged, had off-spooled into the RV dome. The most probable cause was pulling through the cutter bars and wrapping of the tail with zero tension while on orbit. The head end of the Aft stack had wrinkles, creases and foldovers (approximate 28 inches starting 2 feet from head), the most probable cause being film misalignment during manual de-spooling.

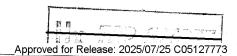
4.3 Optimum Focus Determination

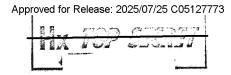
Mission 1209 (SV9/SN12) was launched with focal plane settings of 31 microns on the Forward camera and 70 microns on the Aft camera. Based upon the resolution performance the platen positions for best resolution across the field from readiness test data were 30 microns for the Forward and 75 microns for the Aft camera. These platen positions were corrected for vehicle altitude, gravity effects, and collimator focus as follows:

A plus 14 micron adjustment on both cameras for the altitude shift from infinity (A-2 collimator settings) to 85 nautical miles mission altitude. A minus 15 micron adjustment on the Forward and a minus 19 micron on the Aft camera for the folding flat gravity effects. A plus 2 micron adjustment on the Forward camera to account for a defocus of the test collimator.

Following the evaluation of the on orbit thru-focus tests performed in RV-I no focus change was recommended for either the Forward or Aft cameras. Both the VEM and subjective analysis indicated that both cameras were at optimum focus.

A change in focus of plus 30 microns retreat was implemented on the Aft camera when the material switched from 1414 black and white to the SO-255 conventional color and the SO-130 infrared color material.





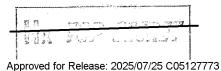
4.4 Optimum OOAA Settings

On-orbit smear data was collected during the second, third and forth mission segments of Mission 1208.

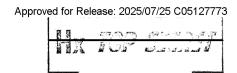
Subjective assessment of smear slit imagery from thru-focus engineering ops 94, 111, 122, 123 and 133 was utilized to evaluate the adequacy of the nominal OOAA settings. Smear slit imagery on the Aft camera untitled edge of the format in the in-track direction showed consistent double imagery with a mean separation of approximately 10 microns, 5.6 microns being due to orbital fixed known errors. The titled edge revealed no in-track image doubling. Both observations are consistent with the skew angle being too large, the equivalent magnitude of the error being approximately 0.041ps. Both subjective evaluation and VEM analysis performed across the format minor axis indicated that the image quality was poorer on the untitled edge than on the titled, corrabonating the smear slit assessment. An OOAA change was implemented to the Aft camera in-track setting of minus four command steps. The Forward camera smear slit imagery in the cross-track direction indicated variable image doubling predominantly indicative of the film velocity being too fast. The variability in the image doubling negated the ability to determine the mean value of the error with a high enough degree of confidence to recommend a change.

Analysis of smear slit imagery from the OOAA engineering ops 212, 217, 240 and 257 verified the minus four command step change implemented to the Aft camera in the in-track direction to be correct. The in-track direction on the Forward camera was determined to be too slow by approximately 0.010ips and the PFA directed a plus one command step change resulting in a new nominal orbital setting of minus two. The cross-track settings on both cameras were determined to be correct.

Since the initial use of smear slits on Mission 1206, all four systems have required an identical change to the Aft camera in-track settings. To date, the possible sources of this residul error in setting the Aft in-track OOAA flight nominal from the ground test sync-flash data have not been determined, and is currently under investigation.



62.



4.5 Optics Thermal Profile

The following subparagraphs describe the thermal environment for Mission 1209. Definitions of measured and calculated temperature parameters are contained in the Mission 1207 Post Flight Report, PM-1496-X. Thermal control for SV-9 can be generally summarized as follows:

 All SS temperatures were within design limits throughout the mission.

4.5.1 SV Environment

SV thermal control parameters are summarized as follows:

• Orbital Elements (Ref. Paragraph 1.5)

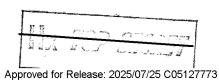
Perigee Altitude	h = 87.7 n.m.
Period	$\tau = 88.8 \text{ min.}$
Inclination	I = 96.6 deg.
Argument of Perigee	$\alpha = 124$ deg.
Beta Range	β = 8.8 deg. (Day 13 β = 12.7 deg. (Day 92

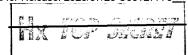
Midsection Thermal Control Design Values

Cocoon		α/ε =	0.359/0.265
Thermal	Baffle	a/ε =	0.90/0.90

• MLI Effective Emittance

Lower 210 Degrees	ε*	Ξ	0.0045
Fwd & Aft Bulkheads	ε¥	=	0.0045
Viewport Baffle	ε*	.22	0.0045
Under TCA Cocoon	ε*	=	0.04
Under SII Coccon	~*	==	0.6





4.5.2 TCA Environment

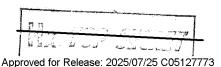
Table 4-1 is a summary of temperature levels, spatial distributions, and temporal variations over a typical orbital revolution in terms of the thermal ICD (1420316A) requirements. Figures 4-6 thru 4-8 show the corresponding orbital profiles of the ICD parameters.

4.5.3 Optical Bar Temperatures

Tref was 71 \pm 3°F, throughout the mission. The equilibrium temperature levels for the A and B optical bars were approximately 71 \pm 3°F respectively. The 3°F tolerances shown for the above nominal values indicate overall shifts in average temperature levels, not random scatter in the data. The shift is attributable to saveral factors including:

- Transition through perihelion and the corresponding variation in insolation.
- o Variable average internal power dissipation related to camera duty cycle.
- o Beta angle changes.

Figure 4-9 shows an orbital profile of the OB temperatures in the stowed position.



64.

	Description	Designated Zones	Max Allowable ICD Value(°f)	Flight Value(°f)		
Ap	Temperature Level Index (T TCA) Zone I Mean Temp. Zone II Mean Temp. Zone III Mean Temp. Zone IV Mean Temp. Forward Bulkhead Middle Bulkhead	Not Applicable	70 [±] 21 N/A N/A N/A N/A N/A N/A N/A	72 72 69 71 75 73 74		
Approved for Release: 2025/07/25 C05127773	Variation of Mean Temp. Between Designated Zones	I to IV II to III I to II III to IV Bulkhead to Bulkhead	9 6 4 4 • 6	3 2 3 3 2 2		
5/07/25 C05127773	Spatial Variation of Time-Average Temp. Measurements at Locations Within Designated Zone	 	11 9 9 11 5 17	542		
	Temporal Variation (Peak to Valley) of Temperature Measurement at any one Location within Designated Zone	 	46 20 20 46 26 57	15 15 4 15		

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5.0 SCF SUPPORT

5.1 TUNITY MISSION 1209

The 'TUNITY software for Mission 1209 performed all of its functions nominally except for the following software problem:

The problem occurred in message 360 on Rev 316 (Op 144). The message contained a mono A operation (Op 143) followed by a stereo operation (Op 144). The mono operation included an automatic focus A ADVANCE only. This was achieved through the use of a SUB card for mono sequences. The return to the null position did not occur until the set-up for the following stereo operation. The SUB card for the mono sequences did not extend that far, therefore, the nominal focus sequence was used and RETREATS for both A and B cameras were commanded. The result was that the focus position of camera A was at the null position but the focus position of B was at plus 2 microns.

5.2 AUGIE

5.2.1 Overall Performance

Real Time performance of Augie met all requirements expected. SSC real time modes are limited to verification of SS status. Playback performance of Augie data met all requirements expected. Time delays for playbacks of data was reasonable with few exceptions.

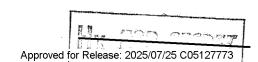
5.2.2 Modifications

Modifications required during flight were made to complete the change requested for the shutter open/close processing and to modify the slit width output processing.

A mode change request has been submitted for the next flight. The change requested is to process the steerer sum error by averageing each second and reporting if this average changes by 5PCM counts from last output.

5.2.3 DTV

SSC utilization of the DTV was limited to passive real time status verification. The use of the DTV will remain limited to status monitoring on the next flight also.



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5.3 RTS Tapes and Microwave

5.3.1 RTS Tapes

The use of RTS tapes was minimal due to reliance on the microwave link capability between the STC and Bldg. 156. RTS tapes met all SSC requirements when used.

5.3.2 Microwave Link

The microwave link into Bldg. 156, its associated terminals and the SSTC were successful in receiving and processing more than 95% of the data transmissions from VTS via the STC. When necessary, unsuccessful data transmissions were either successfully retransmitted post pass, or obtained from a tape dub supplied by the STC ground station.

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HA FOR SECTION

APPENDIX

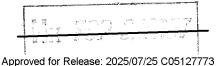
A-1

OPERATIONAL SUMMARY

72.

A. 1209-1

CAMERA OPERATIONS SUMMARY REVS PAD THROUGH REV 307 OP 140. B . PHOTO-FT CUM-TU-FEET REV MSN SCA SCC FRAMES INTEROP FEET OP FAD AFT FWD AFT AFT FWD AFT FWD NUM 160 154 له السَّدة الرقال السامي PRE LO 111/4 PRE LO PRE LO PRE LU J PRE LO PRE LO 3.3 56 C Ü á PRE LO Ć 3.2 Ü PRE LO 7.36 PRE LO ó 3.2 3.3 PRE LO Ó PRE LO PRE LO PRE LO 1)39 3.8 PRE LO PRE LO PRE LO 1+17 -31 PRE LO PRE LO 3.3 ŝΪ PRE LC Ö 0_ PRE LC O. ô 6 126 126 L. 60 -15 4. O 3.3 6.0 -15 3.3 6.0 O -8 3.8 44 1110 1110 137 137 3.0 30 -45 13 120 41) 7.1 60 -30 1.04 1.5 -1 1.7 -25 3.2 3 C 3.8 50 1166 1166 0 144 144 60 -15 2.0



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236 116	90 0	12 12		48 97	
236 117	60 -30	20 20		48 110	
248 118	60 -15	14 14		36 77	77 26457 26474
248 119	30 15	11 11		21 32	32 23518 23527
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285	13C	60	-15	23	23	18	2.7	127	127	28305	23323
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	571 228	50 15	22	2.2	19	27	121	121	13366	11137		
	573 229	30 30	7	7	28	20	ري		13414			
Acres Mari	573 230	90 0	26	26	33	49	211		13658			
	575 23%	30 45	2.6	8.5	49	32	82		13788			
	575 232	60 30	10	10	Zl	29	55		13864			
og Jeslens	576 233	30 45	34	34	28	20	99	99	13331	11753		

αΛΕ <i>1</i>	107777		·		:"		:	4.3	7,5 C				:
CU5.	127773			Αр	proved	for Rel	ease: 202	25/07/25	C0512777	3 BIF-007/D-00	17-75		
	576 234	30 45	11	11	14	14	32	32	14037	11799			
	576 235	30 45	25	25	1.3	13	73	- 73	14123	11085	description of the same same	to the second second second	Account :
, idea,	576 236	30 -15	4	4	13	14	12	22	14148	21911 - ,	own to the		
	577 237	60 -30	8	а	23	30	44	44	14213	11985	700	أفح تستندنسي وسدحان	
	578 238	30 30	28	28	30	20	81	81	14324	12036 1144	,		
	582 239	60 15	4	4	21	3 ù	22			12138			
Stores	582 24C	30 15	7	7	30	22	20	20	14417	12180			
	582 241	30 15	17	17	13	12	49	49	14479	12241			
	589 242	30 30	16	16	13	14	46		14538				
years	590 243	60 -30	26	0	22	Ü	143		14703				
	590 244	90 0	52	52	48	50	421	421	15172	12772			
	591 245	90 15	31	31	55	65	251		15439				
poliumar	592 246	90 -15	32	32	66	68	259	259	15814	13415			
	592 247	30 15	11	11	49	32	32		15895				
	595 248	30 30	7	7	1.3	13	2.0		15928				
	595 249	30 36	7	7	14	14	20		15962				
postin	599 250	30 - 30	6,6;	L. L.	13	14	128		16103				
	599 251	90 0	18	18	33	48	146		16282				
	600 252	30 45	8	8	46	30	23		10351				
-const-	604 253	90 0	25	O	33	.0	203		16587				
	605 254	30 -15	1,6	16	48	15	46		16681				
	608 255	60 -15	14	14	20	29	77		16778				
	614 256	60 - 15	12	12	36	35	66		16880				
	616 257	30 -15	6	6	23	21	17		16925				
	622 258	30 O	1.6	0	13	O	46		16984				
	622 259	60 -15	10	10	29	28	55		17058				
yana.	623 260	60 -30	38	38	34	34	209		17311				
'	625 261	60 15	22	22	35	33	121		17467				
	626 262	30 30	<u> 1</u> 9	19	27	20	55		17349				
(##L)	629 263	30 -45	11	11	21	±2	32		17592				
	632 264	30 -30	4	4	13	13	7.2	12	17617	14054			
	639 265	90 -15	38	38	32	47	303		17957				
printing.	640 266	30 -3C	10	10	47	32	2.9		18033				
	641 267	60 30	56	56	21	2.7	308		18362				
	641 268	30 15	21	21	28	27	6l		16451				
ğerden;	641 269	30 -30	15	15	1.3	14	44		18508				
	654 27C	60 15	34	34	23	28	187		18716				
	655 271	60 15	25	25	35	35	138		18889				
	656 272	60 15	28	28	35	35	154		73010				
your.	657 273	90 Č	10	10	47	55 58	48		19282				
	658 274	30 30	10	0.1	47	31	29	200	19717	10020 14072			
	664 275	90 0	50	50	32	47	403		19802				
Potton	67C 276	30 -30	13	13	47	33 9.4	3.8 an		19830				
	672 277	30 -15	7	7	14	14	20 29		19379				
	673 278	30 30	10	10	14	13	141		20033				,
pody	680 279	30 -30	50	50	13	14	20		20055				
	681 280	30 30	7	7	14	13	88		20176				
	685 283	60 -15	16 20	16	21 35	29 36	105		20376				
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	686 283	6¢ ¢	í	(21	20	ンフ		EUTJE				

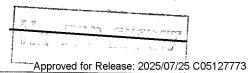
C05	127773			· · · · · · · · · · · · · · · · · · ·	:: ::	·		: "			V.		· 녹지다 왕의
005	12///			Арр	proved		ease: 20	25/07/25	C0512777	3 BIF-0	07/D-0	017-75	
	687 284	90 15	16	16	48	55	130			17891			
	687 285	30 -30	24	24	47	33	70			17994			The first special section represents to the control section of the control of the
ſ	688 286	30 15	19	19	14	1.3	55			18062		200 m 12 mg	2
	688 287	30 30	7	7	13	٤3	20			18095	4. 2.4	H - 3	Markey continued and
\$	638 208	30 0	5	5	13	13	1,5			18123			
i <u>nişe</u>	688 289	30 15	22	22	13	1.3	54			18200			
	690 290	90 15	38	38	32	47	308			18555			
	691 291 691 292	30 -30	8 43	8 43	47	33 13	23 125		21354	18749			
della i	691 293	30 30 30 36	**************************************	6	15	13	17		21535				
	692 294	30 -30	10	10	13	14	29		21577				
	702 295	30 -45	26	26	£3	15	75		23 665				
garatti :	702 296	30 -30	45	45	14	14	131		21810				
	703 297	60 15	16	16	22	29	88		21920				
	766 298	30 0	4	4	28	žó	12		21,960				
	706 299	60 0	60	6Ŭ	21	29	330		22311				
*****	766 300	30 15	7	7	28	20	20		22359				
	721 301	30 30	46	46	13	23	133		22505				
	721 302	60 15	20	20	20	23	110		22635				
imm.	722 303	90 0	23	23	46	54	180		22867				
	729 304	60 0	26	26	44	46	143		23054				
	734 305	00 -15	16	16	3.5	3.5	88		23177				
· jernene	735 306	60 30	24	24	36	35	132		23345				
	735 307	30 0	29	29	28	21	84		23457				
	735 308	3C -30	39	39	13	14	113		23583				
	736 309	30 -30	10	16	14	2.4	46		23643				
	737 31C	60 15	31	31	22	28	173		23836				
i	739 311	60 - 15	17	17	36	3.8	94		23966				
	744 322	90 0	1.7	2.7	48	54	138	138	24152	21422			
jet-o	753 313	30 30	23	2.3	47	3%	57	67	24266	21520			
	754 314	60 -15	13	13	21	29	72		24359				
	755 315	60 15	47	47	35	35	259		24653				
*****	755 316	30 0	9	9	29	23	26		24708				
	766 317	30 30	7	7	11	11	2.0		24739				
	767 318	30 C	4	4	2.2	12	1.2		24763				
leases.	767 319	30 -30	7	7	23	14	0.5		24796				
	769 320	60 0	7		22	29	39		24857				
	772 321	30 -15	4	4	29	22	1.2	3.2	24898				
per la	776 322	90 15	31	31	30	44	251		25179	22448			
	777 323	30 -15	-6		43	29	17		25239	22494			
	778 324 782 325	60 30	23	23	22	28	72		25333				
Politica	783 326	60 15 30 30	22 37	22	31	31	121		25435				
73011	786 327	30 30 30 30	33		23	16	107		25615				
	768 328	30 30	*3	13 13	23 13	i 3 i 3	38 38		25666 25717				*
	788 329	30 30	1.9		五分	1.4	55		25786				
, colors	793 33C	30 15	13		14	15	38		25833				
	794 331	30 15	5	5	14	13	15		25'867				
	798 332	60 -15	15		16	24	83		25966				
*Silvena	800 333	30 15	22		24	16	64		26054				
	्राज्य च च च च		Spine, Shipp	4 A	f	SER SE	- 1			WW			

C05	127	773	. 1									: "	ety talaket		
000	12/	113			*	Aı	pproved	for Re	lease: 20	25/07/25	C051277	73			
	800	334	30	Ö	17	17	23	13	49			23370	BIF	-007/D-0017-75	
	106	335	30	15	16	16	13	1.3				23429			
,-0%.	801	336	30	15	25	25	13	13	73			23515			
	802		3.0	30	25	2.5	13	13	7.3			23601		and the state of t	
		338	30		14	14	13	14	41			23656		gentral years of the Australia	0.9
		339	30	15	10	20	44	1.3	29			23598	S. Carrier	- Branch - Barmara and Baran	فظرانا
,7 ¹⁰ %	802		30	15	7	7	13	23	20			23731			
		3-1	30		16	16	13	14	46			23791	1		employe
	864		60	C	îc	10	22	29	55			23875			
pang.		343		-15	19	19	36	3.6	105			24016			
	818		90	O	18	18	44	52	146			24214			
			30	15	47	47	45	29	136			24379			
Stiribus		346		-30	26	26	13	13	75			24467			
		347	30	30	13	1.3	1.3	13	38			24518			
		348		-15	11	11	34	50	89			24657			
		34.9	60	15	23	13	55	47	72			24776			
Parker		35C	60	30	11	11	34	34	61		27609				
		35%	6.0	15	21	21	36	35	116			25022			
		352	60	-15	13	13	34	36	72			25130			
- Seminar		353	30	Ö	4	4	28	19	12		27907				
		354	30	-15	4	4	13	14	12		27932				
	837	355	90	O	17	17	31	46	138		28101				
Hillians		356	30	30	20	20	40	3.0	53		28205				
i	852	357	30	45	6	6	1.3	13			28235				
	853	358	30	30	13	3.3	14	13	38		28287				
		359	60	С	13	13	6.5	30	72		28379				
emment,			30	Ö	5		29	20	15		28423				
		361	30	-15	5	6	13	13	17		28453				
		302	90	0	28	28	33	49	227		28713				
-mayory;	833	363		-15	38	38	55	48	209		28977				
		364	60	Ö	٧9	19	36	35	105		29118				
	885	365	9.0	Ü	19	19	47	55	254		29319			τ	
****	886		60	õ	1.2	11.	55	47	72		29445	1.00			
	"										1				

A. 1209-3

B. CAMERA OPERATIONS SUMMARY REV 886 OP 366 THROUGH REV 1356 OP 550

REV	MSN OP	SCA	scc	FRA	MES	INT	RCP	РНО	TÖ-FT	CUM-TI	J-FEET			
	NUM			FWD	AFT			FWD	AFT	FWO	AFT	41.4	700	المنافعة المنافعة المنافعة المنافعة
836		50	0	6	7	G	Э	33	39	33	39			The district constitution of the
899	-	30	45	19	0	91	O	55	0	179	39			
900		60	0	32	32	20	99	176	176	375	3 4			
9.02		.60	-1.5	٤6	26	36	35	143	143	554	493			
908		30	15	8	8	29	21	23	6.5	606	537			
912		60	15	19	19	22	29	105	105	733	671			
913		30	45	19	O	23	0	55	0	316	671			
	73 ۋ	6 C	Ç	37	37	ڈے	Зć	204	204	1041	91î			
914		60	30	15	3	36	Ö	83	0	1100	911			
914		90	0	10	10	47	55	81	81	1238	1048			
914	37c	30	30	37	37	47	31	107	107	1442	1186			
915	377	60	3.0	37	37	20	27	204	204	1666	1417			
918	378	60	15	19	19	36	37	105	105	1807	1559			
931	379	60	15	19	Ō	35	Ü	105	0	2947	1559			
931	38°C	60	15	10	20	36	36	55	55	2038	1650			
938	381	3.0	30	13	13	27	19	38	3.8	2103	1707			
950	382	6.C	15	2 C	O	19	Э	55	0	2377	1707			
962	383	60	-15	14	14	34	29	77	77	2238	1813			
963	384	50	15	31	31	37	35	171	171	2496	2019			
966	385	30	Ó	10	10	28	21	46	46	2570	2086			
965	386	90	-15	19	19	29	46	154	154	2753	2286			
967	387	30	30	22	22	45	23	54	64	2862	2378			
958	388	30	. 0	7	7	13	1,3	20	20	2895	243.3			
971	369	90	0	16	2.6	32	48	130	130	3057	2589			
979	39C	90	0	19	19	65	65	154	154	3276	2808			
986	391	30	15	4	4	46	30	2.2	12	3334	2350			
380	392	3.0	0	25	25	13	13	73	73	3420	2936			
993	393	3.0	-45	53	53	13	14	154	154	3587	3104			
9.94	394	30	30	7	7	24	13	20	20	3621	3137			
994	395	30	-30	5	5	23	14	15	15	3649	3166			
9.95	396	3.0	-30	7	7	14	14	20	20	3683	3200			
996	397	60	30	7	7	2.2	23	39	39	3744	3257			
999	398	30	30	19	19	28	2.7	55	55	3827	3343			
959	399	30	Ō	26	26	13	14	75	75	3915	3432			
1011	400	90	15	8	8	31	46	65	65	4011	3543			
2012	401	120	C	44	44	81	89	473	471	4563	4103			
1.013	402	60	15	19	19	78	62	1.05	105	4746	4270			
	403	30	3 C	8	8	28	20	23	23	4797	4313			
1014		30	30	13	13	13	13	38	38	4848	4354			
	405	30	25	7	7	1.3	14	20	20	4881	4393			
1.Cle		30	-30	7	7	14	4.6	20	25	4915	4432			
1019		60	15	19	19	19	26	105	1 C 5	5039	4563			



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	$J\perp ZI$	/ /	5				Approv	ed for R	Release: 2	:025/07/2	25 C05127	773BIF-0	07/0 -0	017-75		
	1025	408	90	0	16	Э	43	C	130	0	5212	4563				
	1028		90	15	34	0	65	0	275	0	5552	4563	-			
,/ma	2031		60	-15	19	19	54	34	105	105	5711	4702	na	KEND EN	as on give s	
	1031		90	0:	18	18	49	56	146	146	5906	4904	1 *7			
	1033		30	15	7	7	48	32	20	20	5974	4956	h 3 34.	34 h. A	Berley S	2 49 -34
		413	90	C	10	10	33	49	81	81	6088	5086	1			
ess ^(T)	1044		60	0	2.2	22	55	48	121	121	6264	5255				
	1044			-15	43	43	36	35	237	237	6537	5528				
	1C44			-30	33	33	35	35	182	182	6754	5745				
independent.	1045		30	15	4	4	29	20	12	1.2	6795	5777				
	1047			-30	16	1.5	14	14	40	46	6855	5337				
	1049		90	15	20	20	32	48	1.62	1.02	7.049	6047				
		420	90	0	1.3	13	58	69	105	105	7222	6221				
NOTE:		423	60	Ö	7	7		48	39	39	7317	6308				
				-15	1.7	17	36	36	94	94	7447	6438				
	1059						ol	76	193	193		6707				
,610PMs	1060			0	18	18		104	503	503	8308	7314				
	1061			. 0	47		104		94	94	8481	7471				
	7.095	425	50	0	17	17	79	63			8567	7550				
	1062			-45	20	20	28	21	58	5.8		7683				
20405641	1063			-30	19	1.9	20	28	105	1.05	8592					
	-	428	60	O	2.8	28	35	34	154	154	8881	7871				
	1077	429	6.0	0	7	7	3 ć	36	39	39	8956	7946	· · · · · · · · · · · · · · · · · · ·	and the second second		
	2078	430	30	-45	10	10	28	21	29	29	9013	7996				
	1078	431	60	15	15	15	21	28	83	83	9117	8107				
	1079	432	30	45	10	10	23	2,0	29	29	9174	8156				
		433	30	15	7	7	13	1.3	20	20	9207	8189				
States		434	6 C	-30	17	17	21	3.0	94	94	9.322	8313				
	2092		30	15	1.6	15	29	20	46	46	9397	8379				
	1092		3 C	30	32	32	13	13	93	93	9503	8485				
	1093			Ü	26	26	49	73	2.78	278	9830	8336				
	1094		6 C	ă	38	38	83	64	209	209	10119	9109				
	1094			-30	14	14	28	21	42		10188	9171				
	1094			-15	6	6.	14	13	1.7		10219	9201				
-17759	1094		30	45	51	51	13	1.2	148		10380	93.51				
			3.0	45	19	19	13	24	55		10448	9430				
	1095			-30	25	25	14	15	73		10535	9518				
.HHvs.	1095					32	15	13	93		10643	9624				
	1095		30	45	32	5	21	31	28		10692	9633				
	1.096			-30	5			20	46		10767	9749				
	1096		30.	0	16	16	29		49		10329	9311				
subdes	1096		30	45	A.7	17	1.3	13			10922	9912		2.		
	1101		60		13	23	< l	29	72							
	1705			-15	19	13	37	38	105		11064					
1-505/1	1108		90	0	47	4	46	53	3.2		11162					
	1108		30	30	46	46	46	30	133		12951					
	1111		50	C	10	10	21	29	55	55	11397	10387				
	1112		90	Ü.	31	31	47	56	252		13695					
portion	1113	454	30	-30	47	47	48	32	15€		11879					
	1114	455	30	-25	37	37	14	14	107		12000					
	1123		60	15	59	59	22	28	321		12343					
proth	1.1.25		90	0	28	28	48	57	226	226	12617	11615				

\sim 0	512	フワワ	3		*							*		
	\mathcal{I}	1 1 1	5				Approv	ed for F	Release: 2	2025/07/	25 C05127	773 ^{BTF-(}	007/D -00	17-75
	1129	453	90	0	26	26	66	55	210	210	12893	11391		
		459	30	0	7	7	47	31	20	20	12960	11942		
	1144		90	0	59	59	33	49	475	475	13468	12406	<u>n</u>	
	1157	463	90	ō		11	67	67	89	89	13624	12622	117	FINE PARTY
	1159			-15	31	31	55	48	171	171	13850	12341	2 3 3 8	H Con
	2160		30	30	13	13	29	20	38	38	13917	12899	<u>L</u>	
similar	1173		60	15	10	10	2.	29	5.5	55	13993	12982		
	1173			-15	8	8	28	22	23		14044			
	1173		90	0	6	5	3%	45	49		14124			
****	1174	+57	50	15	19	19	54	46	105	105	14233	13272		
	1175		60	25	13	13	36	36	72	72	14371	13380		
	1175			-15	3.0	30	36	37	165	165	14592	13582		
	1177		50	-15	8	8	36	36	44	44	14672	13562		
-,	1177		90	ō	41	41	48	55	332	332	15052	14049		
		472	90	õ	28	23	58	69	227	227	15347	14345		
	1190		30	30	20	20	48	32	58	58	15453	14435		
gentled.	1390		60		14	14	2.0	29	77	77	1,5550	14541		
	1192		60	30	40	40	36	35	220	220	15306	14796		
	1193		90	Õ	33	33	48	56	267		16121			
2019/15mm	1194		60	30	16	16	55	47	38		16264			
	1194		90	Ü	1,5	19	49	5.8	154	154	15467	15466		
	1197		90	ō	13	13	55	54	105	105	15627	15625		
	1200		120	0	47	47	6.5	74	503	503	17196	16202		
emetros.	1205			-3 0	29	29	69	46	84		17349			
	1207		30	0	4	4	14	23	12		17375			
	1207			-3C	5	Ś	13	14	1.5		17403			
29-maps		484	60	30	27	27	22	28	149		17574			
	1209		30	15	44	46	28	21	128		17730			
	1207		90		38	38	32	49	3°C8		18070			
******	1209			-15	33	33	53	45	182		18305			
	1210		60	30	19	19	34	32	105	1.05	18444	17433		
	1215			-15	17	17	35	37	94	96	18573	17554		
	1223	707 756	9.0	้อ์	26	26	45	53	211		18830			
_60000		493		-1.5	39	39	52	45	23.5		19097			
	1239		90	15	34	34	47	53	275		19419			
	1239			-30	23	23	4.5	32	67		19532			
Jacque,	1239		60	-30 C	12	12	22	29	6.6		19620			
	1241	495	30	30	17	27	28	20	49		19597			
	12-11	490		-15	30	30	13	14	87		19797			
. is . 195s	1241	457	30	-30	10	10	15	15	29		19841			
		498	60	15	17	17	21	23	94		19956			
	1241	490	30	ب ن	5	5	29	21	15		20000			
	1241	サブブ	20	, U			6 /	Kar 49r	* **		20000			

1243 500

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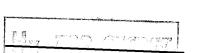
$C \cap$	512	777	٦					1 1.1111	:**:		<i>></i>	**************************************
) <u> </u>	, , ,	_					ed for R	telease: 20	025/07/2	25 C05127	773
	1265		30	-30	7	7	14	24	20	20	21778	20761
	2270	509	60	1.5	22	2.2	2.2	29	121	121	21921	
باشد	1271	51.0	30	30	22	22	23	23	64	64	22013	20995
	1274	544	30	-30	19	19	13	14	55	55	22081	21064
	1274	512	50	15	43	43	21	28	237	237	22339	21329
Sheri	2274	57.3	60	3,0	23	23	36	35	127	127	22502	21491
	1275	514	90	15	92	92	45	53	745	745	23292	22289
	1281	515	30	-15	9	9	47	33	26	26	23365	22348
	1285	516	60	0	12	12	21	28	66	66	23452	22442
promp.	1286	517	90	-15	4	4	47	56	32	32	23531	22530
	1290	518	60	-30	16	16	58	50	88	88	23677	22668
	1290	519	120	0	29	29	60	74	310	310	24047	23052
rub	1291	520	90	0	65	65	84	77	527	527	24658	23656
	1297	521	30	-15	5	5	48	33	15	1.5	24721	23704
	1303	522	90	-C	40	40	33	43	324	324	25078	24076
	1304	523	3.0	Ü	13	13	47	3.2	38	38	25163	24145
	1304	524	60	-15	36	36	21	29	198	198	25382	24372
	1305	525	6.0	-30	11	11	36	37	61	61	25479	24470
	1307	526	60	-15	3.0	30	37	36	1.65	165	25681	24671
. Hitseler	1313	527	30	0	5	5	28	2.0	25	15	25724	24706
	1319	528	3 C	-30	41	42	13	14	119	119	25856	24839
	1319	529	30	-30	17	17	15	14	49	49	25920	24902
passac	1320	53C	30	15	31	31	13	13	90	90	26023	25005
, >	1321	531	60	-15	17	17	21	29	94	94	26138	25128
	1321	532	30	-45	41	41	29	21	119	119	26286	25268
	1322	533	3.0	30	13	13	13	13	38		26337	25319
7 mm	1323	534	60	-15	2.7	17	2%	29	94	94	26452	25442
	1335	535	90	0	8	3	47	55	65	65	26564	25562
	1335	536	90	0	11	11	65	65	89	6.8	26718	25716
Amej	1336	537	60	15	29	29	55	47	100	160	26933	25923
	1338	538	30	30	10	10	28	20	29		26990	25972
	1339	539	30	15	7	7	1.3	13	20	2.0	27023	26005
,i	1339	54L	90	0	43	43	34	5 û	346	348	27405	26403-
	1345	541	30	15	6	ò	47	3 1	17	17	27469	26451
	1351	542	60	15	7	7	21	28	39	39	27529	26518
	1352	543	6.0	0	10	10	36	37	55	5.5	27620	26510
,,,,,,,,	1352	54.4		-30	19	19	28	23	55	55	27703	26686
	1353	545		-15	Ĭ 3	13	22	29	72	72	27797	26787
	1,353	54.6	30	. 0	7	7	28	2.0	20	20	27845	26827
mion.	1354	547		-45	7	7	14	15	20	20	27879	26852
	1355	548	9.0	0	34	34	34	49	275	275	26188	27186
	1356	549	30	30	10	10	47	33	29	29	28264	27246
	1356	550		-15	41	40	21	29	226	219	28510	27494
					. 20							

BIF-007/D-0017-75

A. 1209-4

CAMERA OPERATIONS SUMMARY REV 1356 OP 550 THROUGH REV 2090 OP 759

REV	MSN	SC4	SCC	FRA	4ES	INTE	EROP ET	РНО:	TO-FT	CUM-TU	J-FEET
	NUM			FWD	AFT	FWD	AFT	FWC	AFT	FWD	4FT
588623449916679900671223378 357890004444444422233378 1111111111111111111111111111111111	PM 55123456789C123456789C123456	60000000000000000000000000000000000000	-15505005005055555005555005555 -1555005505555550055555005555	FWO 445873080786370192056474260		FWD 3992026567628558858441917259	TAF 0017226664188665573639172960			FWD 22 308 352 49 5732 847 1058 9768 11768	
1445533555666556444444444444444444444444	5778901234555555555555555555555555555555555555	60 60 90 50 60 60 60 60 60 60 60 60 60 60 60 60 60	130550505055555 - 131335354415	16986577343917743	16986573440917743	22 23 44 28 5 2 2 2 2 2 1 2 3 4 1 2 6 1 2 2 2 2 2 1 1 2 3 6 1	2318524080804305 2222213535	38 55 154 88 203 94 125 132 87 270 32 20 77	88 55 154 68 203 94 125 132 27 27 20 20 77	3596 3679 3679 36773 4262 4673 4573 4673 5172 5204 5467	36077 36779 36779 398375 4687 4687 4687 5137 5204 5311 5472



Approved for Release: 2025/07/25 C05127773

\sim 0	5107772)	"	. "		****			7 77					. . .
CU	5127773)			Δ	pprove	d for Re	elease: 20	025/07/2	5 C051277	73 BIF-00	07/D -00	017-75	
	1484 592	30	30	7	7	28	20	20	20	5515	5513			
	1485 593	6 C	30	25	25	21	29	138	138	5674	5680		······································	1
gena	1485 594	30	15	8	3	23	2.0	23	23	5725	5723	The state of	5745.79	<u>Carrier</u> years
	1487 595	60	0	4	41	21	30	226	226	5972	5979	11.4	dit was not	Land Company
	1497 596	60	30	19	19	37	35	105	105	6114	6119			1
	1493 597	30	30	22	22	28	21	64	64	6206	6204	b		***************************************
Articl.	1498 598	90	O	32	32	33	49	259	259	6498	6512			
	1500 599	60	-30	10	CZ	55	48	55	55	6608	6615			
	1500 600	30	15	4	4	30	21	12	12	6650	6648			
inner	1501 601	60	15	16	16	7.8	26	88	88	6756	6762			
	1502 602	30	-30	28	28	26	§ 9	31	31	6863	6862			
	1506 603	30	-45	4	4	14	14	12	1.2	6889	6888			
-delicate	1513 604	6 ¢	0	Ιū	1.0	2.2	29	55	55	6966	6972			
	1513 605		-15	20	20	29	23	5.8	58	7053	7051			
	1514 506	90	-15	11	11	3.2	49	89	89	71.74	7189			
	1514 607		-15	13	13	43	32	3.8	38	7260	7259			
08980	1514 609		-30	12	1.2	13	13	3.5	35	73.08	7307			
	1514 609	30	-30	7	7	14	14	20	20	7342	7341			
	1517 610	90	15	7	7	33	47	57	57	7432	7445			
; 	1517 611	30	-30	17	1.7	47	32	49	49	7528	7526			
	1517 612		-30	33	33	13	14	95	96	7637	7639			
	1518 513	30	-30	10	10	14	14	29	29	7630	7579			
******	1529 614	60	15	23	13	25	28	72	72	7774	7779			
	1530 515	30	0	13	13	28	21	38	38	7840	7838			
	1530 616	3.0	-30	4	4	13	14	12	12	7865	7854			
	1532 617	30	٥	7	7	14	13	20	20	7899	7897			
address.	1533 518	60	-25	35	35	21	30	193	193	8113	8120			
	1533 619	60	-30	24	24	37	37	132	132	8282	8289			
	1534 620	90	Õ	41	41	49	56	332	332	8663	8677			
v.000cm	1534 621	3 G	15	54	4	48	3.2	12	12	8723	8721			
	1540 622	30	-30	13	23	13	13	3.8	38	8774	8772			
	1546 623	30	15	24	2.4	13	٤3	7 C	7 G	8857	8355			
se ^{re} tare	1546 624		-15	30	30	13	13	8.7	87	8957	8955			
	1547 625	30	-30	44	4, 44	1.3	13	128	128	9098	9096			
	2548 526	30	30	19	19	13	4.3	55	55	91.66	9164			
	1548 527		-30	11	11	21	30	63	62	9248	9255			
	1548 628	30	15	7.7	11	29	20	32	32	9309	9307			
	1549 629	30	0	2,	4	ڏ ڏ	13	12	12	9334	9332			
	1550 63C	90	Û	110	110	31	47	891		10256	10270			
,4900m.	1555 631		-15	5	5	47	32	1.5			10317			
	1562 632	90	15	2 c		34	50	211			10578			
	1563 633	50	15	26	16	56	46	88		10707				
gyrere;	1564 634	3.0	45	3.0	10	23	27	2.9		10764				
:	1564 635		-30	5	5	13	13	1,5		10792				
	1565 636		-15	1.6	16	33	13	46		10851				
er ⁽⁴⁾ sc	1565 637	60	15	11	1.2	21	28	61		10933				
	1566 538	90	0	98	98	4.7	55	794		11774				
	1567 639	90	C	10	16	66	55	130		11970				
	1571 64C	-	- 30	8	3	48	32	23		12041				
3000A1	1579 641	30	-15	13	1.3	1.3	13	38	28	12072	VEDAO			

5612 661

2612 662

1613 563

1614 664

1615 565

1616 066

1621 567

1627 668

1628 669

1628 67C

630 67%

1631 578

1632 673

2636 674

1657 675

1543 676

8644 677

1.644 678

1644 679

1845 580

1647 631

1647 682

1647 003

1648 684

164€ 685

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1665 639

1668 590

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Approved for Release: 2025/	/07/25 C051	27773

J51 <i>Z /</i>	//	۲ .									
30127	, ,	_			- 1	Approve	ed for R	elease: 20	025/07/2	25 C051277	773
1579	642	60	0	11	11	24	32	6%	61	12177	12183
	643	60	-15	23	23	36	36	227	127	12340	12346
	644	60	õ	26	25	36	35	143	143	12519	12525
1580	o4.5	30	-45	26	26	28	20	75	75	12622	12620
1582	646	6 C	-30	56	56	21	30	308	308	12951	12958
	647	6 Û	-15	19	19	27	3.5	105	105	13093	13099
1583	54.8	30	-30	47	→7	28	21	130	136	13257	13256
1583	645	3.0	30	21	21	14	15	61	o L	13332	13332
	65 C	90	U	44	44	32	48	356	356	13723	13736
1995	55i.	60	30	25	ð	53	0	138	O	13911	13736
1595	652	60	-15	10	10	36	47	55	55	14002	13636
1597	653	60	Ú	31	32	36	36	171	171	14239	14045
1598	554	30	30	34	34	28	20	99	99	14336	14104
1598	655	30	-45	22	22	14	14	64	64	14414	14242
1598	656	30	0	7	7	13	13	20	20	1447	14275
1599	657	120	0.	68	68	47	71	720	728	15222	15074
1599	558	90	Ü	69	69	38	83	559	559	15859	15713
2500	659	60	-30	4	4	55	48	22	22	15946	15783
	66 C	6 C	¥ 5.	13	13	36	34	72	72	10054	15889

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73 16154 15982

73 16241 16068

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20 18157 17547

89 18289 17635

20 18577 17956

50 18648 18037

23 18700 18080

121 18841 18230

0 19097 18230

88 19442 18353

300 19786 16706

162 20010 18929

462 20537 19455

29 20612 19515

26 21045 19948

0 21311 19948

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ألمنه تسداد لوانيه الأراسية 1 400 G G NA

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	5127	/ / /	3			,	Approve	ed for R	elease: 2	025/07/2	25 C05127	773
	1679	692	30	-15	4	4	29	22	11	11	21977	20581
	1.680	693	90	0	70	70	33	49	567	567	22577	21197
	1681	694	50	1.5	22	22	55	4.7	120	120	22752	21354
:	1684	695	90	0	16	16	37	47	130	130	22919	21541
	1635	696		-30	4	4	38	23	15	1.2	22969	21576
	1692	697	90	Ü	35	35	33	48	232	282	23284	21906
a	1693	698	30	15	7	7	46	30	20	20	23350	21956
	1693	699	50	15	16	16	21	29	87	87	23458	22072
		70C	50 50	36	13	13	35	35	71	71	23554	22178
contract.	1696			-15 -15	6	5	35	35	33	33	23632	22246
	1696	701		-45	11	11	27	20	32	32	23691	22298
	1700	702					13	13	íž	1.2	23716	22323
	1701	703		-15	4	4 4		29	60	60	23797	22412
desiden	171C	704		-30	11	11	21			89	23934	22556
	1728	705		-15	ii	11	48	55	89		24034	22648
	1735	766		- 30	8	ð	56	48	44	44	24191	22804
	1741	707	60	Ü	24	22	36	33	121	121		
	1744	708	60	15	10	10	34	34	55	55	24280	22893
	1745	709	60	15	19	33	3.5	3.5	105	105	24420	23033
	1745	71 C	60	0	7	7	35	36	39	39	24495	23108
-	1759	711	60	15	13	13	24	34	72	72	24591	23214
	2762	712	90	0	18	18	44	52	146	2.46	24781	25412
	1769	713	120	C	11	11	44	51	118	118	24943	23581
	177-	716.	60	15	13	13	Lydy	29	7.2	72	25059	23682
	1775	715		-30	16	16	28	Si	46	46	25133	23749
	1777	726	90	Ō	62	62	32	47	502	502	25667	24298
	1777	72.7		-15	2.7	17	54	47	94	94	25815	24439
	1778	718	90	ō	26	26	47	54	21.1	211	26073	24704
	1792	729	30	30	10	10	46	30	29	29	26148	24763
	1793	72.0		-30	16	16	20	29	88	88	26256	24380
	1793	721		-3C	7	7	28	20	25	20	26304	
	1794	722	9.0	Q	32	32	33	48	259	259	26595	25227
		723	30	45	13	13	46	30	3.8	38	26680	25295
	1,800			-15	7	7	21	2.9	39	39	26740	25363
indetto.	1804	724				22	36	36	121	121	26897	25520
	1810	725		-15	22	13	28	21	38	38	26963	25579
	1816	726		-45	1.3	7		13	20	20	26997	25612
personal contract of the contr	1826	727	30	30	7		14			55	27072	25695
	1842	728	60	0	10	10	20	28	55 77	77	27183	25807
	1842	729		-30	24	14	34	35			27234	
	1863	736		-45	8	-8	28	0.5	23	23		25850
	1881	731		-15	13	13	22	29	72	72	27328	25951
	1886	732		-30	7	7	23	21	20	20	27376	25992
	1887	733		- 30	14	1 4	14	14	42	41	27431	26347
	1390	734	30	30	7	7	14	13	20	20	27465	
	1906	735		-30	4	l_{γ}	13	1.3	15	12	27490	261.05
	1907	736	30	-30	-5	5	15	15	13	7.4	27518	
	1907	737	60	15	22	22	22	28	121	121	27661	26283
.compu.	1907	738	30	-30	19	7.3	23	20	55	55	27744	26358
	1940	739	60	0	§ 9	29	53	29	105	1 C 5	27870	
	1546		30	45	13	13	2.8	20	38	38		26550
(many)	1951		30	30	I_{i}	4	23	13	12	12	27961	26575

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00	0 1 2 7 7 7	•				Approv	ed for F	Release:	2025/07/	25 C05127	7773 BIE-007/01 -0017-75	
	1955 742	6.0	-15	10	10	21	29	55	55	28037	26659 F-007/D -0017-75	
	1972 743	3.0	30	10	Ü	28	0	29	0	28094	26659	
igua-	1988 744	30	-15	7	7	13	21	2.0	20	28127	26700	
	2003 745	30	15	4	4	14	13	12	22	28153	26725	
	2004 746	30	30	10	10	13	13	29	29	28,95	26767	*
and:	2004 747	30	15	4	4	£3	13	2.2	1.2	23220	26792	-
	2010 748	30	45	7	7	13	13	20	20	28 253	25925	
	2020 749	30	0	1.3	13	14	14	38	38	28305	26877	
	2327 75C	50	15	13	13	21	29	72	7.2	28398	26978	
MINAMA.	2031 751	60	-15	13	13	3 ć	36	72	. 72	28506	27036	
	2033 752	3 C	3.0	i 9	19	28	20	55	55	28589	27161	
	2053 753	60	15	7	7	20	28	38	38	28647	27227	
	2069 754	60	15	10	10	35	35	55	55	28737	27317	
	2084 755	60	35	22	22	34	34	121	121	28892	27472	
	2084 756	30	-45	8	8	23	20	23	23	28943	27515	
	2086 757	60	15	13	10	22	29	72	55	29036	27599	
	2088 758	30	4.5	7	O	11	9	20	0	29067	27599	
	2090 759	60	Ü	16	ũ	20	0	88	O	29175	27599	
w.,	CONSTANT	VEL(CITY	(PREP	21	00	60	ĵ.	0	29235	27659	
	- 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1											